

IFS DOCUMENTATION – Cy48r1 Operational implementation 27 June 2023

PART VIII: ATMOSPHERIC COMPOSITION

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REVISION HISTORY



Chapter 1

Introduction

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The simulation of greenhouse gases (GHG) and reactive trace gases and aerosol (COMPO) is a configurable extension of the IFS. These configuration are used in the operational forecast and reanalysis applications of the IFS for the Copernicus Atmosphere Monitoring Service (CAMS). This part of the documentation describes the simulation of the sink and source processes of atmospheric composition with the IFS as well as the specifics of the data assimilation approach for atmospheric composition.

The other parts of IFS documentation also cover tracer related aspects such as transport, radiation and data assimilation. In this part (8), we will refer to the respective parts. The transport by advection is described in Part III Dynamics and Numerical Procedures. Only aspects specific to tracer advection such as the application of global mass fixers are covered in this part (8). The transport of tracers by turbulent diffusion and convection and the use of prognostic aerosols and ozone in the IFS radiation scheme are documented in Part IV Physical processes.

Atmospheric composition is simulated "on-line" in the IFS, i.e. together with the simulation of the dynamical and physical processes using the same data flow, methods and routines as applied for the meteorological tracers such as cloud water and humidity. This means that each forecast or analysis of the IFS with atmospheric composition also provides a meteorological forecast or analysis. The online approach enables a close coupling between meteorological and atmospheric composition processes. It also makes it possible to use the data assimilation capability of the IFS to assimilate atmospheric composition observations to correct the simulated concentrations.

1.1 BACKGROUND

Monitoring and forecasting of global atmospheric composition are key objectives of the Copernicus Atmosphere Monitoring Service (CAMS), which is implemented by ECMWF on behalf of the European Commission (Peuch *et al.*, 2022). Starting in the early 2000, the IFS has been extended for the simulation of reactive trace gases (Flemming *et al.*, 2015; Huijnen *et al.*, 2016), aerosols (Morcrette *et al.*, 2009; Rémy *et al.*, 2019, 2022) and greenhouse gases (Agustí-Panareda *et al.*, 2014). The on-line approach for the reactive trace gases superseded a two-way coupled system consisting of the IFS and Chemical Transport Models (Flemming *et al.*, 2009). First attempts to assimilate stratospheric ozone at ECMWF started in the late 1990, using a linear parameterization to describe stratospheric ozone chemistry (Part IV Physical processes, Chapter 9). The simulation and assimilation of stratospheric ozone in that way is part of the Numerical Weather Prediction (NWP) applications of the IFS. Up to the previous cycle (CY47R3), also the COMPO configuration of the IFS applied only the linear parameterization to describe stratospheric ozone. CY48R1 is the first cycle that uses an explicit chemical mechanism to simulate chemistry in the stratosphere.



With the capacity to simulate atmospheric composition in the IFS in place, the 4D-VAR data assimilation method of the IFS could be extended to allow the assimilation of satellite retrieved aerosol optical depth (AOD) (Benedetti *et al.*, 2009), reactive trace gases (Inness *et al.*, 2015) and longer-lived greenhouse gases (Engelen *et al.*, 2009; Massart *et al.*, 2014).

The IFS-COMPO configuration has been used to provide global forecasts of atmospheric composition since 2007 (Flemming *et al.*, 2017b) and in an operational mode since 2014. A further application of IFS-COMPO and IFS-GHG is the production of multi-decadal re-analysis data sets of aerosol, reactive trace gases (Inness *et al.*, 2013; Flemming *et al.*, 2017a; Inness *et al.*, 2019) and of greenhouse gases (Agusti-Panareda *et al.*, 2023). The re-analyses are produced by assimilating a wide range of satellite retrieved products of atmospheric composition starting in 2003. The latest version of the reanalysis (EAC4) is being continued to the present date. EAC4 is produced with IFS-COMPO of CY42R1.

The development of the atmospheric composition aspects in the IFS is a joint effort between ECWMF and other European research institutions, including several meteorological services of ECMWF member states. The joint development approach is pursued by implementing a range of chemistry schemes (Huijnen *et al.*, 2019) and other alternative approaches for the description of aerosol processes. Following the approach of the IFS documentation for other components, only the schemes applied in the operational CAMS forecasting system of CY48R1 will be documented here. There are two operational configurations of the CAMS forecasts (o-suites):

- (i) reactive gases and aerosols using the COMPO tropospheric and stratospheric chemistry schemes and the AER aerosol scheme (IFS-COMPO o-suite, resolution: TL511).
- (ii) greenhouse gases CO₂ and CH₄ (GHG) only at increased resolution (IFS-GHG o-suite, resolution: fc TCO1279, analysis TCO399).

1.2 STRUCTURE OF THE DOCUMENTATION

Part 8 (Atmospheric Composition) documents the scientific basis and implementation of the following processes and diagnostics in the IFS in the following chapters:

- Chapter 1: Basic principles of atmospheric composition simulation with the IFS (this section).
- Chapter 2: Chemical and aerosol conversion in the atmosphere.
- Chapter 3: Surface fluxes of atmospheric composition including emissions and removal of atmospheric trace gases and aerosols by deposition.
- Chapter 4: Transport of trace gases and aerosols.
- Chapter 5: Calculation of aerosol radiative variables and other diagnostics.
- Chapter 6: Data assimilation of atmospheric composition retrievals.

For processes and methods that are commonly applied in the IFS for NWP, COMPO and GHG applications, such as transport of tracers or the data assimilation approach, this document will describe the specifics for the application for COMPO/GHG and will refer for the common aspects to the respective parts of IFS documentation.

1.3 FUNDAMENTALS

1.3.1 Continuity equation for tracers

Running the IFS-COMPO suite adds 123 tracers for reactive gases and 16 tracers for various aerosol species to the simulated 3D fields of any NWP application. While the IFS-GHG suite only requires 2 additional tracers. The change of the mass mixing ratio (MMR) $C_A[kg/kg]$ of a tracer A in each grid box is simulated using the 3D continuity equation:

$$\frac{\partial C_A}{\partial t} + \vec{v} \nabla C_i - \frac{1}{\rho} \frac{\partial}{\partial z} K_z \frac{\partial C_A}{\partial z} = \frac{1}{\rho} (R_A + E_A - D_A)$$
(1.1)



The change of C_A is caused by transport processes and source and sink processes. The source and sink processes of tracer A are the emissions and surface fluxes (E_A), the loss by wet and dry deposition (D_A) and its chemical conversion (R_A). The emissions are either external data sets or are simulated online. The loss by wet or dry deposition D_A depends on the environmental conditions and the surface properties and the MMR of the tracer itself. The chemical or aerosol conversion term can either be a source or sink for A. The simulation of this term is a major contribution to the complexity of the atmospheric composition simulation because the chemical conversion of a gas or aerosol component A depends on the concentration of other tracers B, C, D, ..., which introduces a coupling between the simulation of the different tracers.

The transport of C_A is described by the advection with the grid-resolved 3D wind vector \vec{v} and by turbulent diffusion. In the IFS only the vertical turbulent diffusion is considered, which is calculated from the vertical turbulent exchange coefficient K_z and the vertical tracer gradient. A further transport process is the vertical motion of a tracer as part of the convective mass fluxes, which are parameterised as part of the IFS convection scheme.

1.3.2 Simulation of chemical conversion

This section covers the basic principles of the chemical kinetics as an introduction for readers with a non-chemistry background.

For a chemical (bi-molecular) reaction of species A with species B to produce species C and D:

$$A + B \to C + D \tag{1.2}$$

the resulting chemical reaction rate, i.e. the change in time of the volume mixing ratios (VMR) of the reacting species (X_A , X_B) and of the product species (X_C , X_D), is given by the product of the volume mixing ratio of the reacting species (X_A , X_B) and the reaction rate constant k_{AB} :

$$-\frac{dX_A}{dt} = -\frac{dX_B}{dt} = \frac{dX_C}{dt} = \frac{dX_D}{dt} = k_{AB} \times X_A \times X_B$$
 (1.3)

The reaction rate constant k_{AB} depends on the molecular properties of the reactants and on temperature and pressure. Reaction rate constants are determined by laboratory measurements and theoretical considerations and have a varying degree of uncertainty. The VMR of a species A (X_A) is given by the ratio of the number of molecules of A ([A]) and the number of molecules of air per volume unit.

A special case or a simplified version of bi-molecular reactions are mono-molecular conversions $A \rightarrow B$, which take place without the interaction with other reactants. The first-order rate of change depends in this case only on X_A :

$$\frac{X_A}{dt} = -k_A \times X_A \tag{1.4}$$

which can be solved analytically, using the initial volume mixing ratio of *A*:

$$X_A(t) = X_A(t=0)e^{-k_A t} (1.5)$$

Examples of the first-order reaction process are the radioactive decay of Radon, aerosol ageing, unimolecular decay and photolysis. The inverse of the constant k_A can be considered as the e-folding lifetime of species A. The concept of the lifetime can be extented to an atmospheric lifetime of a species by assuming that species reacting with that species remain constant and can therefore become part of a first-order reaction rate.

Photolysis is the breakup of molecules by solar radiation into often unstable products. Photolysis is an important initiator for many chemical reaction chains and cycles in the atmosphere. The photolytic rate constant kj depends on the characteristic properties of the species (quantum yield, absorption cross section) and the actinic radiative flux in the atmosphere.



A chemical mechanism, or chemical scheme, is a set of chemical species and set of chemical reactions between the species or their photolytic decay. It is defined by the (i) list of species and (ii) the specific reaction rate constants or photolytic rate constants and their dependency on temperature and radiation.

1.3.3 Units and measures of concentrations

The tracer concentrations are simulated as mass mixing ratios (MMR) in the IFS, which is the same approach as used for specific humidity. The MMR of tracer A (C_A) is given by the mass (m_A) of A with respect to the total mass of air (m_{air}) in each grid cell:

$$C_A = \frac{m_A}{m_{oir}} \tag{1.6}$$

Because the mass of air in each grid cell is proportional to the vertical extend of the grid cell in pressure units Δp , the mass of tracer A (m_A) can be calculated using the gravitational constant G and the grid box area S in the following way:

$$m_A = C_A \frac{\Delta p}{G} S \tag{1.7}$$

The volume mixing ratio (X, unit= $\frac{mol}{mol}$) of A is the ratio of the number molecules of A ([A]) and the number molecules of air ([air]). It can be calculated for gases from MMRs (C_A) using the molar mass of A (M_A) and of air (M_{air}) in the following way:

$$X_A = \frac{[A]}{[air]} = C_A \frac{M_{air}}{M_A} \tag{1.8}$$

In most cases taking into account only the molecular weight of dry air $(M_{air-dry} = 0.029 \frac{kg}{mol})$ is sufficient but more accurate conversions need to consider the impact of the specific humidity q on M_{air} .

The mass concentration of A $(c_A$, unit = $\frac{kg}{m^3}$) is defined as the tracer mass m_A per volume. It can be calculated from C_A by the multiplication with the density of air (ρ_{air})

$$c_A = C_A \rho_{air} \tag{1.9}$$

 ρ_{air} depends on the pressure, temperature and humidity (Part IV Physical processes).

The scaling of X_A and c_A to commonly used units such as ppb (parts per billion) and $\frac{\mu g}{m^3}$ is achieved by the multiplication with 10^9 .

1.4 OVERVIEW OF THE CODE

The simulation of atmospheric composition tracers follows the treatment of other grid-point variables such as humidity. The sink and source processes and the transport by vertical turbulent diffusion and convection are included in the physics parameterization package (CALLPAR Part IV Physical processes, Section 1.2). The simulation of prognostic variables, i.e. also the prognostic tracer fields, in the physics only allows the consideration of dependencies in the vertical dimension.

The input to the physics (CALLPAR) are the MMR of the prognostic tracers (grid-box mean) and the tendencies from the advection calculated by the dynamics. The tendencies from the different sink and source processes and the turbulent and convective transport are computed in separate routines called from CALLPAR.

The tendencies from the different processes and the advection are added together. The MMR entering these routines are intermittently updated with the accumulated tendency from the previous process ('method of fractional steps'). This approach to operator splitting introduces a dependency on the order of the different source and sink routines in CALLPAR.



At the end of CALLPAR, the accumulated tendencies of the physics and the tendencies from the advection are added and consequently applied to the initial MMR entering the physics to calculate the MMR of the next time step. A check of the total tendencies to avoid MMR below a "chemical zero" of 1.0×10^{-25} [kg/kg] is carried out.

The sink and source process for reactive gases and aerosol are simulated in separate routines because they have been developed independently. The further harmonisation of the aerosol, chemistry and GHG routines is a ongoing development effort. For GHG the emissions and the turbulent and convective transport are simulated in the physics. The only sink process for GHG is the application of a climatology of CH_4 loss rates.

In CALLPAR, the following high-level atmospheric composition routines are called in the following order:

COMPO_ APPLY_EMISSIONS Computes surfaces fluxes from sector specific input data and applies

diurnal cycles and application of elevated emissions (see section

3.1.1)

CHEM_INI Initialisation of chemical scheme

AER_INI Calculation of online-emissions for sea salt and dust, and aerosol dry

deposition and sedimentation velocities

CONVECTION_LAYER convection as part of physics package includes convective transport

of tracers

TURBULENCE_LAYER turbulence as part of physics package, includes vertical diffusion

of tracers with injection of surface fluxes and calculation of dry deposition velocities using input from the land surface scheme

LIGHTNING_LAYER lightning parameterization part of physics package, includes

calculation of NO_x lightning emissions

CHEM_MAIN calculation of chemical conversions and wet deposition of reactive

gases, applies methane loss rates (GHG) and NO_x lightning

emissions

AER_PHY3 calculation of secondary aerosol formation, wet deposition of

aerosols and aerosol optical diagnostics (AOD, PM, etc.)

The MMR and respective tendencies of chemical species (from CHEM_MAIN) required for the calculation of secondary aerosol formation in AER_PHY3 are stored in the array PCHEM2AERO.

1.5 CONFIGURATION OF ATMOSPHERIC COMPOSITION IN THE IFS

The simulation of atmospheric composition with the IFS allows many different options for the choice of the simulated greenhouse gases, reactive gases and aerosol tracers and their properties. There is the choice of one of several chemistry schemes of varying complexity (MOCAGE, MOZART, RnPb, linear CO) and the number of the considered aerosol tracers.

GHG, aerosols and reactive gases can be simulated together or separately. If aerosols are run without a chemistry, there are options available to account for a simplified treatment of secondary aerosol formation (sulphates) without the need to simulate the gas-phase chemistry.

This document only describes the configuration used by CAMS for (i) the IFS-COMPO operational system of CY48R1, which applies the COMPO tropospheric scheme (based on the CB05 scheme), the COMPO stratospheric chemistry scheme (based on the BASCOE scheme) and the AER aerosol scheme or (ii) the IFS-GHG configuration (only CO_2 and CH_4).

The IFS is configured by means of namelists. These fortran namelists are compiled by the run time environment (ifs scripts) based on variables set in prepIFS. Important prepIFS variables are LMACC=true to trigger the treatment of atmospheric composition, LCHEM=true to trigger the calculation of chemistry, LAER=true to trigger the simulation of aerosols and LGHG=true to trigger the simulation of greenhouse gases.

The following IFS namelists are used to configure the atmospheric composition simulation in the IFS.



NAMGFL

Specification of all GFL fields; lists each simulated tracer field and specifies the advection and mass fixing options. Additionally it specifies if chemistry tracers

are subject to dry and wet deposition

NAM_COMPO NAM_CHEM NAEAER NAMCOMPO_EMIS configuration options valid for all tracers, and for secondary aerosol formation

configuration of the chemistry simulation

configuration of the aerosol simulation and properties of every aerosol tracer

configuration of the sectoral emission input



Chapter 2

Conversion of aerosols and trace gases in the atmosphere

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Appendix A. Chemistry Species Tables

The chemical conversion of atmospheric trace gases occurs by the cumulative influence of photolysis, bimolecular reactions between gaseous components, and heterogeneous reactions of gases on the surface of cloud and aerosol particles. Beside the gas-phase chemical conversion, condensable trace gases undergo homogeneous nucleation or heterogeneous condensation on existing aerosol particles to form secondary aerosols, with specific processes that form organic and inorganic aerosol types.

The resulting rate of change of the mass mixing ratios of trace gases and aerosols is simulated by one of several chemical mechanism of the IFS. The various chemical mechanisms differ in the selection of the considered chemical species, photolytic, homogeneous and heterogeneous reactions and in the calculation of the respective rates of each of these processes based on the environmental conditions such as temperature, radiation and presence of aerosols and clouds. The numerical formulation of a chemical mechanism is a large and often numerically stiff system of ordinary differential equations, which require the application of dedicated mathematical solvers.

Atmospheric aerosol consists of a multitude of components with variable sizes and shapes. Major natural aerosol components are sea salt and dust particles. Further important aerosol types from a variety of natural, biogenic and anthropogenic sources are primary and secondary organic and inorganic aerosols as well as black carbon.

Some of these aerosol particles undergo ageing, while secondary aerosol particles can change due to chemical conversion and volatility.

Trace gases and aerosol can also dissolve in cloud and rain drops depending on their degree of solubility, where aqueous-phase reactions lead to further chemical processing determining the fractional partitioning between the gas and aerosol phase. A dedicated module for aqueous (wet) phase chemistry and gas-aerosol partitioning simulates these processes.



The atmospheric chemistry module used in IFS-COMPO (CY48R1) consists of a tropospheric and stratospheric chemistry scheme, supplemented with tracers supporting secondary aerosol formation. In total this results in 123 tracers active in the chemistry module. The switch between the application of the tropospheric and stratospheric chemistry schemes is applied at the tropopause, the height of which is diagnosed from the temperature lapse rate in the IFS. The atmospheric aerosol module (AER) in IFS-COMPO CY48R1 consists of 16 species, which are in various ways coupled to the atmospheric chemistry.

2.1 TROPOSPHERIC CHEMISTRY

The tropospheric chemistry used in IFS-COMPO CY48R1 has evolved and expanded over time. It originates from the Carbon Bond mechanism version 5 (CB05) (Yarwood *et al.*, 2005) as formulated for regional air-quality studies, but has been tailored and modified for use in the Chemistry Transport Model TM5 (Williams *et al.*, 2013; Huijnen *et al.*, 2010). The scheme was first implemented in IFS as documented in Flemming *et al.* (2015). The CB05 mechanism designed by Yarwood *et al.* (2005) is characterized by a lumping approach for organic species, i.e. by defining a separate tracer species for specific types of functional groups. The original CB05 scheme implemented in the IFS has gradually been expanded particularly to include more explicit organic chemistry. The complete list of trace gases in the model is given in Tables A.1-A.4. This encompasses trace gases and reactions that describe basic inorganic chemistry and simple organic chemistry responsible for carbon monoxide and methane oxidation (Table A.1), as well as reactions that describe volatile organic compounds (VOCs, Table A.2).

2.1.1 Inorganic chemistry

Basic inorganic chemistry is modeled by the trace gases specified in Table A.1. For application in IFS-COMPO the inorganic chemistry has been extended with NO_y species including $CH_3O_2NO_2$ (Williams *et al.*, 2017; Huijnen *et al.*, 2019). The IFS-COMPO chemistry includes a sulphur cycle, represented by sulphur dioxide (SO₂), di-methyl sulphide (DMS) and methyl sulphonic acid (MSA), as well as ammonia (NH₃) chemistry (Huijnen *et al.*, 2010). This is coupled to inorganic aerosol formation. From CY48R1 onwards, both hydrogen cyanide (HCN) and acetonitrile (CH₃CN) are included as long-lived tracers indicative of biomass burning activity.

2.1.2 Chemistry of degradation of organic compounds

Basic reactions describing the oxidation of CO and CH₄ are modeled using trace gases as defined in Table A.1. Oxidation up to C3 organic species is treated explicitly, following chemistry mechanism extensions developed in the context of TM5 and IFS-COMPO, as described in Williams *et al.* (2013, 2017); Huijnen *et al.* (2019). The trace gases involved here are given in Table A.2. This includes lumped tracers for specific types of functional groups which are used to model the oxidation of higher volatile organic compounds, such as butane (C4), pentanes (C5), and (higher) aldehydes.

From CY48R1 onwards the basic isoprene oxidation scheme has been replaced using a more explicit approach based on Stavrakou *et al.* (2010), which has been further modified according to Lamarque *et al.* (2012) and Myriokefalitakis *et al.* (2020). Reaction products from this isoprene oxidation scheme include glyoxal (CHOCHO), glycolaldehyde, isoprene-peroxide, hydroxy-acetone and two hydroxy-aldehydes, as documented in Williams *et al.* (2022).

Basic aromatic chemistry is described through the inclusion of lumped xylene and toluene tracers and their oxidation reaction chain. These reaction products are coupled with secondary organic aerosol (SOA) formation as described below. For this purpose, three gas-phase SOA precursor tracers, referred to as SOGs, are defined.

2.1.3 Mechanism version, reaction rates, and solver

The IFS-COMPO tropospheric chemistry version in CY48R1 is referenced as *tc*06*g*. It uses a chemistry table file tm5_ver19.x, but run in conjunction with IFS-COMPO stratospheric chemistry the table file is bascoetm5_ver6.x. Including SOA precursor tracers, this mechanism consists of 71 trace gases that are



active in the tropospheric chemistry, while it has 157 gas-phase reactions, 3 heterogeneous reactions and 2 aqueous phase reactions. The reaction rates follow the recommendations given in either Burkholder *et al.* (2020) or the latest recommendations by IUPAC, as hosted at http://iupac.pole-ether.fr.

The tropospheric chemistry is solved based on Kinetic PreProcessor (KPP) routines, using the four stages and third-order Rosenbrock solver (Sandu and Sander, 2006).

2.1.4 Photolysis

For parameterization of the photolysis rates the separate approaches for troposphere and stratosphere are retained, as these have been optimized in the past for these specific applications. The modified band approach (MBA) is adopted for the computation of tropospheric photolysis rates (Williams *et al.*, 2006, 2012). It computes net photolysis rates based on 7 absorption bands across the spectral range 202 - 695 nm. For instances of large solar zenith angles (71-85°) a different set of band intervals is used to avoid introducing large biases. The radiative transfer calculation is performed with a two-stream solver using the absorption and scattering components introduced by gases, aerosols and clouds, computed on-line for each of the predefined band intervals.

In the configuration with coupled tropospheric and stratospheric chemistry the photolysis rates for reactions occurring both in the troposphere and stratosphere are merged at the interface, in order to ensure a smooth transition between the tropospheric and stratospheric parameterizations. This is done by an interpolation at four model levels around the interface level between both parameterizations, for solar zenith angles (SZA) $< 85^{\circ}$. For larger SZA the original value for the photolysis rate is retained in case of stratospheric chemistry, while it is switched off for the troposphere.

The impact of aerosol on the actinic fluxes required for the calculation of the photolysis rates is simulated using the AOD of the aerosol fields of the aerosol scheme AER in the IFS.

2.1.5 Heterogeneous chemistry

Heterogeneous reactions rates are calculated using the Surface Area Density (SAD) which is provided by AER aerosol model to account for scattering and available surface area for heterogeneous conversion. For N_2O_5 , HO_2 , and NO_3 , the reactions on aerosols are represented as a pseudo-first-order process with reaction rate k_{het} according to:

$$k_{het} = \left(\frac{r}{D_g} + \frac{4}{c\gamma}\right) S \tag{2.1}$$

With D_g being the gas-phase diffusion coefficient of the gaseous species, r the mean aerosol radius, c the mean molecular velocity of the gaseous species, γ the reaction probability of uptake coefficient and S the aerosol surface area density. The γ values used are specified in Table 2.1. Particularly for the uptake of HO₂ the parameterization proposed by Thornton *et al.* (2008) is used, assuming a fixed pH value of 5.5. This results in γ -values ranging between 10^{-4} and 0.1 depending on temperature and ambient HO₂ concentrations.

2.2 ATMOSPHERIC AEROSOL

The aerosol module in the IFS is referred to in literature as AER (Rémy et al., 2022), and is originally derived from the LOA/LMDZ model (Boucher et al., 2002; Reddy et al., 2005). It is essentially a bulk aerosol scheme, while for sea salt aerosol and desert dust, a sectional approach is employed. As such, it is often denoted as a bulk-bin scheme. The aerosol species use mass mixing ratios as the prognostic variable of the aerosol tracers. The prognostic species are sea salt, desert dust, organic matter (OM), black carbon (BC), sulfate, nitrate, ammonium and secondary organic aerosols (SOA). The SOA species has been introduced in CY48R1 with two tracers (biogenic and anthropogenic); before that, SOA was represented as part of the OM species. This means that up to cycle 47R3, the OM species included both primary and secondary aerosols, while in CY48R1 and beyond, it consists only of the primary aerosols.



Table 2.1 γ values used in heterogeneous conversion rates on atmospheric cloud droplets, ice and aerosols. T08 refers to Thornton et al. (2008).

Particle type	$\gamma (N_2O_5)$	γ (HO ₂)	γ (NO ₃)
cloud droplets	$2.7 \times 10^{-5} exp(1800/T)$	-	-
ice particles	$2.7 \times 10^{-5} exp(1800/T)$	0.025	-
desert dust	0.01	0.06	$0.01 ; 10^{-4} \text{ for RH} < 50\%$
sea salt	0.02	T08	0.01
organic matter (hydrophilic)	0.02	T08	0.01
secondary organic aerosol	0.02	T08	-
black carbon (hydrophilic)	0.01	T08	0.01
sulfate	0.02	T08	0.01
ammonium	0.002	T08	0.01
nitrate	0.002	T08	0.01

AER is run coupled to the COMPO tropospheric chemistry scheme in the IFS-COMPO in the operational configuration. As described in Rémy *et al.* (2019), AER can also be run in a stand-alone mode (IFS-AER), i.e. without any interaction with the tropospheric chemistry, in which case the nitrate and ammonium species are not included, and a specific tracer representing sulfur dioxide is subsequently added. When running stand-alone mode, two additional tracers are included, to represent secondary organic anthropogenic and biogenic precursors gases.

The assumed number size distribution specifics are shown in Table 2.2. These are used offline in the Mie code to generate the optical properties: wavelength dependent mass extinction, asymmetry parameter, signgle scattering albedo and lidar ratio for each aerosol species. In the processes that depend on aerosol size, such as dry deposition and for heterogeneous reactions, the mass median diameter (MMD) is used, as computed using the assumed size distribution given in Table 2.2. In CY48R1 the assumed number size distribution of dust has been modified and now uses values provided by Ryder *et al.* (2018) from aircraft measurements over the tropical Eastern Atlantic.

Desert dust is represented with three size bins, with radius bin limits at 0.03, 0.55, 0.9 and 20⁻m. Sea salt aerosol is also represented with three size bins, with radius bin limits of 0.03, 0.5, 5 and 20⁻m at 80% relative humidity. All of the sea salt aerosol parameters (concentration, emission, deposition) are expressed at 80% relative humidity; this is in contrast to the other aerosol species in IFS-AER, which are expressed as dry mixing ratio. The sea salt aerosol mass mixing ratio, as well as the emissions, burden and sink diagnostics, need to be divided by a factor of 4.3 to convert to dry mass mixing ratio in order to account for the hygroscopic growth and change in particle density. There is no mass transfer between bins for either dust or sea salt.

The organic matter and black carbon species consist of their hydrophilic and hydrophobic fractions, with the ageing processes transferring mass from the hydrophobic to hydrophilic components. Sulfate aerosols are represented by one prognostic variable. The nitrate species consists of two prognostic variables that represent fine nitrate produced by gas-particle partitioning and coarse nitrate produced by heterogeneous reactions of dust and sea salt particles. Finally, the secondary organics species consists of two tracers, that represent biogenic and anthropogenic SOA. In all, the AER consist of 16 prognostic variables when running coupled with the COMPO tropospheric chemistry scheme (default). When AER is run without coupling to a chemistry scheme, an additional SO2_SO4 precourser tracer is added for the simulation of sulphates and two precursor gases are added for the simulation of SOA. The simulation of nitrate and ammonium aerosol is not possible without coupling to the chemistry scheme)

2.2.1 Hygroscopic growth and ageing

Hygroscopic growth is the process whereby, for some aerosol species, water is mixed in the aerosol particle, increasing its mass and size and decreasing its density. This process is treated implicitly in IFS-AER, since size is not resolved. It plays an important role, however, in the computation of optical properties and also for sinks that are size and/or density dependent, in particular dry deposition. The species subjected to hygroscopic growth in IFS-AER are sea salt, the hydrophilic components of OM



Table 2.2 *Aerosol species in AER*

Aerosol type	Size bin limits	ρ
	(sphere radius, ⁻m)	$(kg m^{-3})$
	0.03-0.5	
Sea Salt	0.5-5.0	1183
(80% RH)	5.0-20	
	0.03-0.55	
Dust	0.55-0.9	2610
	0.9-20	
Black carbon hydrophobic	0.005-0.5	1000 0
Black carbon hydrophilic	0.005-0.5	1000 0
Organic matter hydrophobic	0.005-20	1300
Organic matter hydrophilic	0.005-20	1300
Sulfates	0.005-20	1760
Nitrate fine	0.03-0.9	1730
Nitrate coarse	0.9-20	1400
Ammonium	0.005-20	1760
biogenic SOA	0.005-20	1800
anthropogenic SOA	0.005-20	1800

and BC, sulfate, nitrate, ammonium and SOA. The amount of water that is mixed in the aerosol particle depends on the particle size. Table 2.3 details the changes in size for the concerned species. The values are drawn from Tang and Munkelwitz (1994) for sea salt, Tang *et al.* (1997) for sulfate and ammonium, /Chin *et al.* (2002) for BC, and Svenningsson *et al.* (2006) for nitrate.

For OM and BC, once emitted, the hydrophobic component is transformed into a hydrophilic one with an exponential lifetime of 2.78 hours. This value has been updated in CY48R1 from 1.1 days in cycle 47R3.

Table 2.3 Hygroscopic growth factor depending on ambient relative humidity.

RH/%	Sea-salt	OM	ВС	Sulfate and Ammonium	Nitrate	SOA
0–40	1	1	1	1	1	1
40–50	1.442	1.	1	1.169	1.1	1.0
50–60	1.555	1.05	1	1.220	1.2	1.2
60–70	1.666	1.1	1	1.282	1.25	1.3
70–80	1.799	1.15	1	1.363	1.3	1.4
80–85	1.988	1.2	1.2	1.485	1.35	1.5
85–90	2.131	1.25	1.3	1.581	1.5	1.6
90–95	2.361	1.3	1.4	1.732	1.7	1.7
95–100	2.876	1.4	1.5	2.085	2.1	1.8

2.2.2 Secondary organic aerosol formation

SOA precursors are included, with the aromatic gas-phase precursors (xylenes, toluene) acting as exclusive anthropogenic and biomass burning sources, using the approach of Karl *et al.* (2009), see also Figure 2.1. In a similar way, the production of a biogenic SOA tracer has been linked to the oxidation of both isoprene and terpenes. For this, we adopted three Secondary Organic aerosol precursor Gas (SOG) classes: two associated to anthropogenic emissions and one associated to biogenic emissions. These precursor gases are linked to the respective anthropogenic and biogenic SOA tracers (two anthropogenic precursor gas tracers contribute to anthropogenic SOA production).

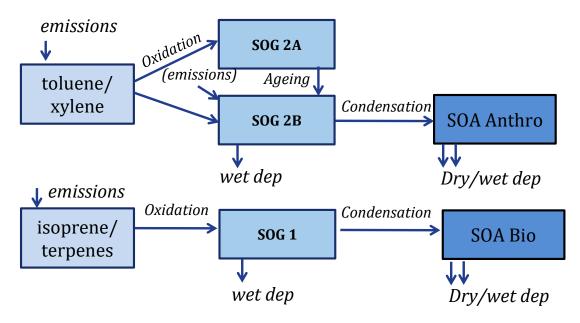


Figure 2.1 Schematic of the secondary organic aerosol module

(a) SOA formation from biogenic sources

In IFS, the modelling of SOA formation from isoprene and terpene oxidation is modeled using a single SOA and SOG family, following the approach proposed by Tsigaridis and Kanakidou (2003). This implies that a single, dominant, low volatility SOG tracer is assumed. Products of VOC oxidation partition between purely gas-phase chemistry and SOG, and its efficiency is described by production yields α and ϵ . The SOG production follows the reactions below:

$$\begin{split} \text{ISOP} + \text{OH} &\longrightarrow \alpha_1 \text{SOG}_1 + (1 - \alpha_1)(0.65 \text{ISOPBO2} + 0.35 \text{ISOPDO2}) \\ \text{ISOP} + \text{O}_3 &\longrightarrow \alpha_2 \text{SOG}_1 \\ &\quad + (1 - \alpha_2)(0.35 \text{PAR} + 0.65 \text{ISPD} + 0.2 \text{XO}_2 + 0.2 \text{C2O3}) \\ &\quad + 0.6 \text{HCHO} + 0.066 \text{HO}_2 \end{split} \tag{2.2}$$

$$\begin{split} \text{TERP} + \text{OH} &\longrightarrow \epsilon_1 \text{SOG}_1 + (1 - \epsilon_1)(5 \text{PAR}) \\ &\quad + 1.25 \text{XO}_2 + 0.25 \text{XO}_2 \text{N} + 1.22 \text{HCHO} \\ &\quad + 0.47 \text{ALD2} + 0.47 \text{CO} + 1.22 \text{HO}_2 \end{split} \tag{2.4}$$

$$\begin{split} \text{TERP} + \text{O}_3 &\longrightarrow \epsilon_2 \text{SOG}_1 + (1 - \epsilon_2)(6\text{PAR}) \\ &+ 0.76\text{XO}_2 + 0.18\text{XO}_2\text{N} + 1.8\text{HCHO} + 0.21\text{ALD2} \\ &+ 0.21\text{CO} + 0.28\text{HO}_2 + 0.57\text{OH} \\ &+ 0.38\text{C2O3} + 0.39\text{CH}_3\text{O}_2 \end{split} \tag{2.5}$$

In this formulation we aim at carbon mass conservation across chemistry and aerosol formation. The standard gas-phase reaction rates are used for these individual reactions of isoprene and terpenes with OH and O₃. Here we neglect night-time aerosol precursor formation from reaction with NO₃, considering that this is a minor channel compared to the other parameterizations (Tsigaridis and Kanakidou, 2003), and considering the high level of simplification already adopted by assuming only a single precursor gas (SOG1). Mass yields (α_1 , α_2 , ϵ_1 , and ϵ_2) are as specified in Table 2.4.



(b) SOA formation from anthropogenic sources

To account for SOA formation from anthropogenic sources, a simplified description of aromatic chemistry has been introduced in the COMPO tropospheric chemistry following Karl *et al.* (2009), through transport and oxidation of toluene and lumped xylenes as described by the reactions below, with mass yields specified in Table 2.4.

$$TOL + OH \longrightarrow \beta_1 SOG2A + \beta_2 SOG2B + (1 - \beta_1 - \beta_2)(5PAR + AROO2)$$
 (2.6)

$$TOL + O_3 \longrightarrow \phi_1 SOG2A + \phi_2 SOG2B + (1 - \phi_1 - \phi_2)(5PAR + AROO2)$$
 (2.7)

$$XYL + OH \longrightarrow \gamma_1 SOG2A + \gamma_2 SOG2B + (1 - \gamma_1 - \gamma_2)(5PAR + AROO2)$$
 (2.8)

$$XYL + O_3 \longrightarrow \chi_1 SOG2A + \chi_2 SOG2B + (1 - \chi_1 - \chi_2)(5PAR + AROO2)$$
 (2.9)

SOG formation from PAR, OLE and C_3H_6 has not been included here, although combined they may contribute significantly (up to 50%) to the SOA production budget, e.g., Tsimpidi *et al.* (2014). Instead, this is parameterized by adding an extra direct emission source to the SOG2B tracer based on the NMVOC emissions. Note that for anthropogenic SOG two classes have been defined: a high-volatility class (SOG2A) and a low-volatility class (SOG2B). Considering that only a single corresponding aerosol type is assumed, all mass in the high-volatility class is assumed to be in the gas-phase. An ageing reaction, combined with a 15% mass accumulation, is introduced for anthropogenic aerosol, where the high-volatility class is converted to the low-volatility class (Tsimpidi *et al.*, 2014), a according to:

$$SOG2A + OH \longrightarrow 1.15 \times SOG2B, k = 9 \times 10^{-12} cm^3 molec^{-1} sec^{-1}$$
(2.10)

(c) Aerosol mass yields

SOG production yields from oxidation reactions are given in Table 2.4. In their specification we loosely follow suggestions for net aerosol mass production yields as reported in the literature (Chung and Seinfeld, 2002; Henze and Seinfeld, 2006; Tsimpidi *et al.*, 2016; Hodzic *et al.*, 2016). For the biogenic SOG yields, the low-NOx conditions are assumed best representative on a global scale, while for anthropogenic aromatics the high-NOx conditions are assumed representative. These yields implicitly account for the mass weight conversion from the precursor VOC gases to the SOG. In a future revision, a more explicit formulation including mass weight factors for precursor gases and SOG will be necessary.

Table 2.4 Secondary aerosol mass yields for various volatility bins in the SOA scheme

Biogenic/Anthropogenic	Reactions	Mass yields	SOG1/SOG2B	SOG2A
2 0		•	C*-Bins 1-10	C*-Bins 100-1000
			$[K=1m^3/\mu g]$	$[K=0.01 \text{m}^3/\mu\text{g}]$
			$[\log(c^*)=0]$	$\log(c^*)=2$
Biogenic	ISOP + OH	α_1	0.05	-
Biogenic	$ISOP + O_3$	α_2	0.1	-
Biogenic	TERP + OH	ϵ_1	0.15	-
Biogenic	$TERP + O_3$	ϵ_2	0.15	-
Anthropogenic	TOL + OH	β_1, β_2	0.3	0.6
Anthropogenic	$TOL + O_3$	ϕ_1,ϕ_2	0.3	0.3
Anthropogenic	XYL + OH	γ_1,γ_2	0.3	0.3
Anthropogenic	$XYL + O_3$	χ_1,χ_2	0.3	0.3



2.2.3 Secondary inorganic aerosol formation

(a) Production of sulfate through oxidation

The oxidation of sulfur dioxide (SO_2) to sulfuric acid (H_2SO_4) in the gas-phase occurs by the reaction with OH as described in Huijnen *et al.* (2010). The reactions involved are:

$$SO_2 + OH + O_2 \longrightarrow SO_3 + HO_2$$
 (2.11)

$$SO_3 + H_2O \longrightarrow H_2SO_4$$
 (2.12)

In the COMPO tropospheric chemistry scheme, SO₃ is not a prognostic species, and the two reactions above are treated as one, which produces sulfuric acid from sulfur dioxide.

(b) Production of sulfate through aqueous phase chemistry

The main source term for the production of H_2SO_4 occurs within cloud droplets, predominately by the oxidation by hydrogen peroxide (H_2O_2) and ozone (O_3). Note that each step in this process is pH dependant. The reactions involved are:

$$SO_2 + H_2O_2 \longrightarrow H_2SO_4$$
 (2.13)

$$SO_2 + O_3 + H_2O \longrightarrow H_2SO_4 + O_2$$
 (2.14)

The cloud droplet pH is calculated by accounting for the dissolution of CO₂ along with the strong acids and bases following (The "a" subscripts stands for aerosol phase, and "g" for gaseous phase):

$$[H^{+}] = 2[SO_{4}]_{a} + [MSA]_{a} - [NH_{4}]_{a} + [HNO_{3}]_{g} + [NO_{3}]_{a}$$
(2.15)

The uptake of SO_2 into droplets is expressed as an effective Henry's law coefficient taking into account the dissociation into bisulphite (HSO_3^-) and sulphite (SO_3^-) thus amplifying the fraction dissolved and available for oxidation, according to:

$$H_{eff}(SO_2) = H(SO_2) \left(1 + \left(\frac{K_{S1}}{[H^+]} + \frac{K_{S1}K_{S2}}{[H^+]^2} \right) \right)$$
 (2.16)

The rate expressions for the aqueous phase SO_2 oxidation are specified in Table 2.5.

Concentrations in the gas-phase are updated accordingly once the extent of oxidation has been calculated, which then is used for the aerosol representation.

Table 2.5 Reaction rate terms used for the description of aqueous phase oxidation

Aq. reaction	Rate expression
$SO_2 + H_2O_2$	$\frac{8.0 \times 10^4 exp \left(-3560 \left(\frac{1}{T} - \frac{1}{298.}\right)\right)}{0.1 + H^+}$
$S(IV) + O_3$	$4.39 \times 10^{11} exp\left(\frac{-4131}{T}\right) + 2.56 \times 10^{3} exp\left(\frac{-966}{T}\right) + \frac{2.56 \times 10^{3} exp\left(\frac{-966}{T}\right)}{H^{+}}$

(c) Production of nitrate and ammonium through gas-particle partitioning

The parameterization of the gas/particle partitioning between nitric acid (HNO₃), nitrate (NO₃⁼) and ammonium (NH₃)/ammonia (NH₄⁺) follows Hauglustaine *et al.* (2014). The most abundant acids in the troposphere are sulfuric acid (H₂SO₄) and nitric acid (HNO₃) (Tilgner *et al.*, 2021). NH₃ acts as the main neutralizing agent for these two species. As a first step, ammonium sulfate is formed from H₂SO₄ and NH₃, only limited by the less abundant of the two species. This reaction takes priority over the formation of ammonium nitrate (NH₄NO₃) because of the low vapour pressure of sulfuric acid. The main reaction



pathways are as follows.

$$NH_3 + H_2SO_4 \longrightarrow (NH_4)HSO_4$$
 (2.17)

$$3NH_3 + 2H_2SO_4 \longrightarrow (NH_4)_3H(SO_4)_2 \tag{2.18}$$

$$2NH_3 + H_2SO_4 \longrightarrow (NH_4)_2HSO_4 \tag{2.19}$$

Following Metzger *et al.* (2002), depending on the relative concentrations of ammonia and sulfate, three domains are considered to characterize how ammonium sulfate is formed. The total ammonia, sulfate, and nitrate concentrations are defined as follows.

$$T_A = [NH_3] + [NH_4]$$
 (2.20)

$$T_{S} = [SO_4] \tag{2.21}$$

$$T_N = [HNO_3] + [NO_3]$$
 (2.22)

For ammonia-rich conditions ($T_A > 2T_S$), Reaction 2.19 is considered. For sulfate-rich conditions ($T_A \leq 2T_S$ and $T_A > T_S$) Reaction 2.18 is considered and for very sulfate-rich conditions ($T_A \leq T_S$) Reaction 2.17 is considered. As a second step, if NH₃ is still present after Reactions 2.17, 2.18 and 2.19, it is used for the neutralization of HNO₃ by the following reaction:

$$NH_3 + HNO_3 \longrightarrow NH_4NO_3$$
 (2.23)

The equilibrium constant K_p of reaction 2.23 depends strongly on relative humidity and temperature. The parameterization of (Mozurkewich, 1993) is used to represent this dependence. Total ammonia that remains after reactions 2.17, 2.18 and 2.19. is written as

$$T_{A}^{*} = T_{A} - \Gamma T_{S}, \tag{2.24}$$

where the value of Γ is 1, 1.5, or 2 depending on whether reactions 2.17, 2.18 and 2.19 took place, respectively. If $T_N T_A^* > K_p$, then ammonium nitrate is formed and its concentration is calculated by:

$$[NH_4NO_3] = 0.5 \left[T_A^* + T_N - \sqrt{(T_N + T_A^*)^2 - 4(T_N T_A^* - K_p)} \right]$$
(2.25)

Otherwise, ammonium nitrate dissociates and the concentrations of both $[NH_4 \text{ and } NO_3 \text{ are null.}]$ Reaction 2.18 also allows us to compute the concentration of NH_3 at equilibrium; the concentration of particulate NH_4^+ is then given by

$$[NH_4] = T_A - [NH_3] \tag{2.26}$$

The concentration of NH₄⁺ is also supplemented by the ammonium from ammonium sulphate.

(d) Production of nitrate and ammonium through heterogeneous reactions

Gaseous HNO₃ can also condense on large particles. The formation of smaller nitrate and ammonium particles through gas-to-particle partitioning is solved before heterogeneous reactions because the equilibrium is reached faster (Hauglustaine *et al.*, 2014). After the smaller particles are in equilibrium, the condensation of HNO₃ on larger particles is treated. Heterogeneous reactions of HNO₃ with calcite (a component of dust aerosol) and sea salt particles are accounted for through the following reactions.

$$HNO_3 + NaCl \longrightarrow NaNO_3 + HCl$$
 (2.27)

$$2HNO_3 + CaCO_3 \longrightarrow Ca(NO_3)_2 + H_2CO_3 \tag{2.28}$$

While the NaCl species is similar to sea salt aerosols, calcite (CaCO₃) is one of the many components of dust aerosol. In Fairlie *et al.* (2010) and Hauglustaine *et al.* (2014), the concentration of calcite is taken as 3 or 5% of the total concentration of dust aerosol. An experimental version of IFS-AER that simulates



a simplified dust mineralogy was used to compute a climatology of airborne calcite using as an input the dataset of Journet *et al.* (2014), which provides an estimate of the calcite content in the clay and silt fraction of soils. This climatology of dust mineralogy has been used to derive a dataset that provides the fraction of airborne dust that is composed of calcite, which is loaded into the IFS from an external file and used here. A 1st-order update parameterization is used to represent the uptake of HNO₃ over sea salt and calcite particles. The rate constants of reactions 2.27 and 2.28 are computed in a simplified way compared to the original scheme of Hauglustaine *et al.* (2014) for each sea salt (SS) and desert dust (DD) bin i:

$$K_{\text{SS}_i} = 4\pi D_{\text{SS}_i}^2 N_{\text{SS}_i} \left(\frac{D_{\text{SS}_i}}{2MDC} + \frac{4}{\nu \gamma} \right)^{-1}$$
 (2.29)

$$K_{\text{DD}_i} = 4\pi D_{\text{DD}_i}^2 N_{\text{DD}_i} \left(\frac{D_{\text{DD}_i}}{2MDC} + \frac{4}{\nu \gamma} \right)^{-1}$$
 (2.30)

where D_{SS_i} is the mass median diameter of sea-salt bin i, D_{DD_i} is the mass median diameter of desert dust bin i, $N_{\mathrm{SS}i}$ and $N_{\mathrm{DD}i}$ are the number concentration of sea-salt and desert dust bin i, respectively, computed using the mass concentration and the mass median diameter. MDC is the pressure and temperature-dependent estimated molecular diffusion coefficient, ν is the temperature-dependent estimated mean molecular speed and γ is the reactive uptake coefficient. For sea-salt, as in Fairlie *et al.* (2010), a dependence of the uptake coefficient on relative humidity is used. Similarly to the gas-to-particle partitioning reactions, the tendency of HNO₃ is updated. The concentration of the desert-dust and sea-salt bins are also updated depending on the amount of coarse mode nitrate that is produced.

2.3 STRATOSPHERIC CHEMISTRY

The stratospheric chemistry module in IFS-COMPO is a re-implementation of the chemical module originally developed for the Belgian Assimilation System for Chemical ObsErvations (Errera *et al.*, 2019, BASCOE) to assimilate satellite observations of stratospheric composition. BASCOE is based on a Chemistry Transport Model (CTM) of the stratosphere which is used to investigate stratospheric photochemistry (Muncaster *et al.*, 2012; Prignon *et al.*, 2021). From the BASCOE system the chemical scheme and the parameterization for Polar Stratospheric Clouds (PSC) has been implemented in the IFS.

The COMPO stratospheric chemical scheme used here is labelled sb15bs. It includes 64 species interacting through 157 gas-phase, 9 heterogeneous and 53 photolytic reactions. The available tracers are defined in Tables A.1 and A.3 This chemical scheme merges the reaction lists developed by Errera and Fonteyn (2001) to carry out data assimilation of stratospheric trace gases with the list included in the SOCRATES 2-D model for long-term studies of the middle atmosphere (Brasseur *et al.*, 2000; Chabrillat and Fonteyn, 2003). The resulting list of species includes all the ozone-depleting substances and greenhouse gases necessary for multi-decadal simulations of the couplings between dynamics and chemistry in the stratosphere, as well as the reservoir and short-lived species necessary for a complete description of stratospheric ozone photochemistry. Gas-phase and heterogeneous reaction rates have been updated to JPL evaluation 18 (Burkholder *et al.*, 2015).

In addition to the original BASCOE chemical scheme, the COMPO stratospheric chemistry module also includes basic sulphur chemistry to represent the formation of gas-phase sulphuric acid and to allow coupling with the sulphate aerosol module. OCS, SO₂, SO₃ and H₂SO₄ are thus included into the scheme sb15bs, using again the chemical rates compiled by JPL (Burkholder *et al.*, 2015) for the five corresponding gas-phase reactions and the photolysis of OCS and SO₃. The photolysis of H₂SO₄ uses the absorption cross-sections reported by Feierabend *et al.* (2006) in the visible wavelength range, Lane and Kjaergaard (2008) at Lyman-alpha as well as the pressure-dependent quantum yields reported by Miller *et al.* (2007).



2.3.1 Photolysis

Lookup tables of photolysis rates are computed by the TUV package (Madronich and Flocke, 1999) as a function of log-pressure altitude, ozone overhead column and solar zenith angle using a spectral grid of 171 wavelength bins covering the spectral range from 116 nm to 735 nm. The photolysis tables used in chemical scheme sb15bs are based on absorption cross-sections from JPL evaluation 17 (Sander *et al.*, 2011), while the solar spectral irradiance is based on the daily SSI dataset from CMIP6 as published by (Matthes *et al.*, 2017). The official CMIP6 dataset is a compromise (mean spectra) between the empirical model NRLSSI2 and the semiempirical model SATIRE. It covers the years 1850 to 2014 and is extended with forecasts for the years 2015 to 2299.

It is also possible to compute photolysis rates fully online using the same TUV package. While this leads to significant increases in computational costs it was demonstrated that this results in significant improvements for stratospheric ozone especially in the polar regions.

A special case is the photolysis rate of NO_2 , for which the tropospheric photolysis module (MBA, see above) is used to calculate the photolysis also for the stratosphere. An advantage is that this module considers the albedo of the surface and of clouds.

2.3.2 Heterogeneous chemistry

The kinetic rates for heterogeneous chemistry are determined by the parameterization of Fonteyn and Larsen (1996), using classical expressions for the uptake coefficients on sulfate aerosols (Hanson and Ravishankara, 1994) and on PSCs (Sander, 2000).

The SAD of stratospheric aerosols uses an aerosol number density climatology based on an IFS-CB05BASCOE-GLOMAP experiment. Ice PSCs are presumed to exist at any grid point in the winter/spring polar regions where water vapour partial pressure exceeds the vapour pressure of water ice (Murphy and Koop, 2005).

Nitric Acid Tri-hydrate (NAT) PSCs are assumed when the nitric acid (HNO3) partial pressure exceeds the vapour pressure of condensed HNO3 at the surface of NAT PSC particles (Hanson and Mauersberger, 1988). The surface area density is set to $2\times 10^{-6}~\rm cm^2/cm^3$ for ice PSCs and $2\times 10^{-7}~\rm cm^2/cm^3$ for NAT PSCs. The sedimentation of PSC particles causes denitrification and dehydration. This process is approximated by an exponential decay of HNO3 with a characteristic time scale of 20 days for grid points where NAT particles are assumed to exist, and an exponential decay of HNO3 and H2O with a characteristic time scale of 9 days for grid points where ice particles are supposed to exist. The actual transport to lower levels by sedimentation is not considered.

2.4 BOUNDARY CONDITIONS FOR LONG-LIVED TRACE GASES

Surface boundary conditions for the tracer MMR are imposed for some long-lived stratospheric gases with surface emissions such as CH_4 , N_2O and CFCs. This approach allows to simulate the flux from the troposphere to the stratosphere without the need to simulate the surface emissions of these species.

Meinshausen *et al.* (2017) provide a comprehensive analysis of GHG surface boundary conditions (including the stratospheric source gases) for CMIP6 model simulations as a function of month, year and latitude from pre-industrial times until December 2014. This dataset has been extended from 2015 to 2100 using projections into the future of emissions of greenhouse gases following each of the 9 socioeconomic scenarios provided for the CMIP6 activity (Gidden *et al.*, 2019). We choose the dataset corresponding to the scenario SSP2 4.5, which follows a middle-of-the-road pathway.

For the IFS, a subset of values has been extracted from the combined dataset, at the native 15° latitudinal resolution available between 1995-2030 and encoded in a text datafile (if needed, this can be extended for future climate mode experiments). The surface constraints apply to 15 species, namely: CCl4, CFC11, CFC113, CFC114, CFC115, CFC12, CH₃Br, CH₃CCl₃, CH₃Cl, CH₄, CO₂, ha1211, ha1301, HCFC22 and N₂O.

The CH₄ surface tropospheric mixing ratios are constrained using a time-dependent latitudinal gradient based on monthly-mean observations derived from remote stations, i.e. there is no longitudinal



variability accounted for. The option to use CH₄ emissions is also supported, combined with a smaller relaxation at the surface in case CH₄ itself is not assimilated. Optionally also the CH₄ atmospheric concentrations can be forced to a fixed value or taken from the GHG scheme.

2.5 CLIMATOLOGICAL METHANE LOSS (GHG)

In the GHG configuration of the IFS only CO_2 and CH_4 is simulated. The chemical sink of CH_4 mainly by reaction with OH in the troposphere and the stratosphere is simulated by a climatological loss rate derived from the TM5 model (Krol *et al.*, 2005) optimised with methyl chloroform in the troposphere and the 2-D Max Planck Institute photochemical model in the stratosphere, following Bergamaschi *et al.* (2009). The loss rate is provided as climatological 3D monthly mean data set at a resolution of $3^{\circ} \times 4^{\circ}$.

2.6 CODE OVERVIEW

The IFS-AER aerosol routines are called from AER_PHY2 and AER_PHY3. The routines in AER_PHY2 deal with online emissions (desert dust, sea-salt) and the computation of dry deposition and sedimentation velocities, and will be detailed in Chapter 3. The routines called from AER_PHY3 deal with aerosol conversion processes, wet deposition and optical diagnostics:

AER_CGROWTH conversion of hydrophobic to hydrophilic for OM and BC (called twice) computes nitrate and ammonium from gas-particle conversion and

from heterogeneous reactions

AER_CSCAVL19 aerosol in-cloud and below-cloud wet deposition, called twice

(for large scale and convective precipitations)

AER_BDGTMSS computes aerosol optical diagnostics: AOD, SSA, extinction profiles, etc.

The COMPO atmospheric chemistry module is called from CHEM_MAIN, and is named CHEM_BASCOEMT5. From the BASCOETM5 module a large set of routines are called. Here we list them in their approximate order. The most important routines that drive *stratospheric* chemistry aspects are:

BASCOE_J_INTERP interpolation of photolysis rates used for the stratospheric chemistry module

BASCOE_HETCONST compute heterogeneous reaction rates active in the stratosphere

BASCOE_KPP_RATES compute reaction rates active in stratospheric chemistry

BASCOE_KPP_INITIALIZE map array of trace gases towards array ordering used in KPP-solver

in the stratosphere

BASCOE_KPP_INTEGRATOR call to KPP solver, this updates trace gases due to chemical reactions

in stratosphere

BASCOE_KPP_UPDATE_CIFS_CONC map updated array of trace gases back to standard ordering as used in IFS

BASCOE_PSC_PARAM compute dehydration and denitrification in stratosphere

Apart from the stratospheric photolysis routine these routines are only called for grid boxes which are above the tropopause. The list of the most important routines involved in *tropospheric* chemistry aspects are:



COD_OP_TM5 compute cloud absorption and scattering optical depths as input for

tropospheric photolysis rate computation

compute aerosol absorption and scattering optical depths for TM5_MACC_AEROSOL

tropospheric photolysis rate computation

TM5_PHOTO_FLUX interface routine to compute tropospheric photolysis rates

TM5_WETCHEM_POINT compute aqueous phase chemistry

compute reaction rates (including heterogeneous) active in tropospheric chemistr TM5_CALRATES

TM5_KPP_RATES map reaction rates towards array used in KPP-solver in troposphere

TM5_KPP_INITIALIZE map array of trace gases towards array ordering used in KPP-solver in tropospher

TM5_KPP_INTEGRATOR call to KPP solver, updates trace gases due to chemical reactions in troposphere

TM5_KPP_UPDATE_CIFS_CONC map updated array of trace gases back to standard ordering used in IFS

TM5_SOA call to SOA production routine

TM5_O3S call to simple solver to compute tropospheric ozone loss for O3S tracer

Again, apart from photolysis aspects these are only called for grid boxes that are located below the tropopause.

At the end of the routine CHEM_BASCOETM5, after all processes have been finalized, the updated concentrations of all relevant tracers are converted into chemical tendencies (variable PTENC1), which is the most important output of this module.



APPENDIX A. CHEMISTRY SPECIES TABLES

Table A.1 *Trace gases defined in IFS-COMPO atmospheric chemistry module - p1: basic inorganic and organic chemistry.*

Formula (IFS name)	Trace gas name	Characteristics
О	oxygen atom	chemistry modeled in stratosphere only
O1D	excited oxygen atom	chemistry modeled in stratosphere only
O3	ozone	
H	hydrogen atom	chemistry modeled in stratosphere only
H2	hydrogen	chemistry modeled in stratosphere only
OH	hydroxyl radical	
HO2	hydroperoxy radical	
H2O2	hydrogen peroxide	
H2O	water	chemistry modeled in stratosphere only
		differs from q
N	nitrogen atom	chemistry modeled in stratosphere only
NO	nitrogen monoxide	
NO2	nitrogen dioxide	
NO3	nitrate radical	
HNO3	nitric acid	
HO2NO2	pernitric acid	
N2O5	dinitrogen pentoxide	
N2O	nitrous oxide	chemistry modeled in stratosphere only
PAN	peroxyacetyl nitrate	chemistry modeled in troposphere only
CH3O2NO2	methyl peroxy nitrate	chemistry modeled in troposphere only
HONO	nitrous acid	chemistry modeled in troposphere only
СО	carbonmonoxide	
CO2	carbondioxide	chemistry modeled in stratosphere only
		differs from GHG config.
CH4	methane	differs from GHG config.
CH3O2	methylperoxy radical	Ŭ
CH3OOH	methylperoxide	
CH2O	formaldehyde	
CH3	methyl radical	chemistry modeled in stratosphere only
CH3O	methoxy radical	chemistry modeled in stratosphere only
HCO	formyl radical	chemistry modeled in stratosphere only
HCN	hydrogen cyanide	Marker for biomass burning
CH3CN	acetonitrile	Marker for biomass burning
DMS	dimethyl sulfide	chemistry modeled in troposphere only
SO2	sulfur dioxide	
SO3	sulfur trioxide	
MSA	methanesulfonic acid	chemistry modeled in troposphere only
OCS	carbonyl sulfide	chemistry modeled in stratosphere only
H2SO4	sulfuric acid	chemistry modeled in troposphere only
NH3	ammonia	chemistry modeled in troposphere only
NH2	amine	chemistry modeled in troposphere only



 $\textbf{Table A.2} \ \textit{Trace gases defined in the IFS-COMPO atmospheric chemistry module - p2: non-methane \ \textit{hydrocarbons}.$

Formula (IFS name)	Trace gas name	Characteristics
C2H4	ethene	chemistry modeled in troposphere only
PAR	paraffins	CB05 tracer with single-bond
OLE	olefins	CB05 tracer with double-bond
ALD2	aldehydes	CB05 tracer representing aldehydes
ROOH	peroxides	CB05 tracer representing peroxides
ONIT	organic nitrates	CB05 tracer representing organic nitrates
C2O3	peroxyacetyl radical	chemistry modeled in troposphere only
ROR	organic ethers	CB05 tracer
RXPAR	PAR budget corrector	CB05 tracer
XO2	NO to NO2 operator	CB05 tracer
XO2N	NO to alkyl nitrate	CB05 tracer
СНЗОН	methanol	chemistry modeled in troposphere only
CHOCHO	glyoxal	chemistry modeled in troposphere only
HCOOH	formic acid	chemistry modeled in troposphere only
MCOOH	methacrylic acid	chemistry modeled in troposphere only
C2H6	ethane	chemistry modeled in troposphere only
C2H5OH	ethanol	chemistry modeled in troposphere only
C3H8	propane	chemistry modeled in troposphere only
C3H6	propene	chemistry modeled in troposphere only
CH3COCHO	methyl glyoxal	chemistry modeled in troposphere only
CH3COCH3	acetone	chemistry modeled in troposphere only
ACO2	acetone product	chemistry modeled in troposphere only
HYAC	hydroxyacetone	chemistry modeled in troposphere only
IC3H7O2	IC3H7O2	chemistry modeled in troposphere only
HYPROPO2	HYPROPO2	chemistry modeled in troposphere only
C5H8	isoprene	chemistry modeled in troposphere only
ISPD	methacrolein; MVK	chemistry modeled in troposphere only
ISOPOOH	isoprene hydroperoxides	chemistry modeled in troposphere only
ISOPBO2	Isoprene radical B	chemistry modeled in troposphere only
ISOPDO2	Isoprene radical D	chemistry modeled in troposphere only
HPALD1	hydroperoxy aldehydes type 1	chemistry modeled in troposphere only
HPALD2	hydroperoxy aldehydes type 2	chemistry modeled in troposphere only
GLYALD	glycolaldehyde	chemistry modeled in troposphere only
C10H16	terpenes	chemistry modeled in troposphere only
XYL	xylenes	chemistry modeled in troposphere only
TOL	toluene	chemistry modeled in troposphere only
AROO2	peroxy radical from aromatics	chemistry modeled in troposphere only
SOG1	condensable gas type 1	secondary organic aerosol precursor
SOG2A	condensable gas type 2a	secondary organic aerosol precursor
SOG2B	condensable gas type 2b	secondary organic aerosol precursor



Table A.3 Trace gases defined in the IFS-COMPO atmospheric chemistry module - p3: Stratosphere.

Formula (IFS name)	Trace gas name	Characteristics
CL	chlorine atom	reactive in stratosphere only
CL2	chlorine	reactive in stratosphere only
CH3CL	methyl chloride	reactive in stratosphere only
CLO	chlorine monoxide	reactive in stratosphere only
OCLO	chlorine dioxide	reactive in stratosphere only
CLOO	asym. chlorine dioxide radical	reactive in stratosphere only
HCL	hydrogen chloride	reactive in stratosphere only
HOCL	hypochlorous acid	reactive in stratosphere only
CLNO2	nitryl chloride	reactive in stratosphere only
CLONO2	chlorine nitrate	reactive in stratosphere only
CL2O2	dichlorine dioxide	reactive in stratosphere only
BR	bromine atom	reactive in stratosphere only
BR2	bromine atomic ground state	reactive in stratosphere only
CH3BR	methyl bromide	reactive in stratosphere only
CH2BR2	dibromomethane	reactive in stratosphere only
CHBR3	tribromomethane	reactive in stratosphere only
BRO	bromine monoxide	reactive in stratosphere only
HOBR	hypobromous acid	reactive in stratosphere only
BRCL	bromine monochloride	reactive in stratosphere only
HBR	hydrogen bromide	reactive in stratosphere only
BRONO2	bromine nitrate	reactive in stratosphere only
HF	hydrogen fluoride	reactive in stratosphere only
CCL4	tetrachloromethane	reactive in stratosphere only
CH3CCL3	methyl chloroform	reactive in stratosphere only
CFC11	trichlorofluoromethane	reactive in stratosphere only
CFC12	dichlorodifluoromethane	reactive in stratosphere only
CFC113	trichlorotrifluoroethane	reactive in stratosphere only
CFC114	1 2-dichlorotetrafluoroethane	reactive in stratosphere only
CFC115	chloropentafluoroethane	reactive in stratosphere only
HCFC22	chlorodifluoromethane	reactive in stratosphere only
HA1301	bromotrifluoromethane	reactive in stratosphere only
HA1211	bromochlorodifluoromethane	reactive in stratosphere only

Table A.4 *Trace gases defined in the IFS-COMPO atmospheric chemistry module - p4: Marker tracers.*

Formula (IFS name)	Trace gas name	Characteristics
Rn	radon	fixed lifetime; produces lead
Pb	lead	only wet removal
STRATAER	stratospheric aerosol	reactive in stratosphere only
PSC	polar stratosph cloud	reactive in stratosphere only
O3S	stratospheric ozone	Copy of O3 in stratosphere, only loss in troposphere
NOXA	nitrogen oxides Transp	Family tracer for advection
CLXA	Reactive Chlorine	Family tracer for advection
BRXA	Reactive Bromine	Family tracer for advection



Chapter 3

Surface fluxes of atmospheric composition

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 - 3.2.3 Sedimentation of aerosols
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Emissions are the fluxes of tracer mass from the surface into the atmosphere. Emissions are caused by human activity (anthropogenic emissions), release and uptake processes from the vegetation (biogenic emissions/fluxes) and from the solid earth surface or the oceans (natural emissions/fluxes).

The production of nitrogen monoxide (NO) from lighting activity (3.1.3) that occurs throughout the atmosphere is strictly speaking a chemical conversion (oxidation) of nitrogen. These lightning NO_x emissions are still covered in this section because they are an important source for nitrogen oxides independent of other trace gases.

The removal of the trace gases at the surface is called deposition. Dry deposition occurs by contact with the surface or vegetation at the ground level. Wet deposition is caused by precipitation that removes dissolved trace gases and aerosols. The aerosol and trace gases are dissolved in cloud water or ice (rain out) or captured by rain and snow while precipitating through air (wash out). Sedimentation is the gravity driven downward motion of heavier aerosol particles.

3.1 EMISSIONS AND SURFACE FLUXES

Emission data are provided as gmapped gridded data sets, often called **inventories**, which are processed as input to the IFS simulation. Emission inventories are typically averages over longer time periods such as annual means or monthly means over several years to represent seasonality. Some emissions, which strongly depend on meteorological conditions, are **simulated on-line** at every time-step in the IFS to capture their temporal variability. Currently the IFS simulates on-line the following emissions:

- Saltation of dust aerosol from dust source regions (3.1.2, (a))
- Release of sea salt aerosol over the oceans (3.1.2, (b))
- Biogenic fluxes of CO₂ (3.1.4)

As the simulation of time varying emissions is often too complex to be simulated on-line, at least some aspects of the temporal variability are on-line simulated in IFS such as the application of diurnal profiles (3.1.1, (c)) to the processed inventory emissions.



3.1.1 Emissions from inventories (natural, biogenic, soil and ocean)

The emissions inventories used in the IFS of CY48R1 come from a wide range of data sets and are listed in Table 3.1.

Туре Inventory Species Reference Biomass burning GFAS 1.4 CO, SO_2, NO_x Kaiser et al. (2012) CH₄, CO₂, NH₃, VOCs Anthropogenic CAMS-GLOB-ANT v5.3 CO, SO_2, NO_x Granier et al. (2022) CH₄, CO₂, NH₃, VOCs Aviation CAMS-GLOB-AIR v1.1 CO_2 , NO_x Granier et al. (2022) Denier van der Gon et al. (2021) Biogenic CAMS-GLOB-BIO v3.1 C₅H₈, C₁0H₁₆, VOCs Natural/Ocean CAMS-GLOB-OCE v3.1 DMS Denier van der Gon et al. (2021) Natural/Volcanic Climatology SO₂ Carn et al. (2017) Natural/Ocean **POET** $C_2H_4, C_2H_6,$ Granier et al. (2005) C₃H₆,C₃H₈, CO, NH₃ Natural/Soil ORCHIDEE NO Lathière et al. (2006) Schery (2004) Natural/Soil WMO Rn Biogenic DMS Spiro *et al.* (1992) Natural/Ocean Jena-Carboscope CO₂ Rödenbeck et al. (2013) CH_4 Natural/Termites Climatology Sanderson (1996) Natural/Wild animals CH_4 Houweling et al. (1999) Climatology CH_4 Lambert and Schmidt (1993) Natural/Ocean Climatology Natural/soil Climatology CH_4 Ridgwell et al. (1999) Natural/wetland Climatology CH_4 Spahni et al. (2011)

Table 3.1 *Emission inventory data sets used in CY48R1.*

Most emissions inventory data are provided on a monthly time resolution to capture the seasonal cycle. Only the GFAS-based fire emissions are provided as daily mean values. The anthropogenic emissions include trends based on projections into the future, which allows the use of year-specific monthly-mean emission data. For natural and biogenic emissions monthly-mean climatologies are constructed for the use in most application because timely data is not available.

Outgassing volcanic SO₂ emissions are known to be varying considerably over the years, Therefore a climatology has been constructed based on a recent satellite-based inventory of large emitters (Carn *et al.*, 2017). In this climatology the minimum of the mean value over time, or the trend over the full time series is used, to avoid over-estimating present-day emissions.

The anthropogenic emissions are given for a set of source categories (sectors), that are listed in Table 3.2. The emissions for each anthropogenic sector as well as some of the biomass burning and biogenic emissions are assigned to sector-specific diurnal profile and injection methods, which are also listed in Table 3.2.

Land based biogenic emissions for DMS with a total of approx. 0.9 Tg S yr^{-1} are applied according to Spiro *et al.* (1992).

(a) Emission processing

The emission fields read by the IFS are sector specific (3.2) daily mean fields for each considered species at the horizontal resolution of the IFS valid for the first day of the forecast. Reading the emissions fields separately for each sector and species makes it possible to apply sector-specific diurnal cycle profiles and injection procedures in the IFS. The external pre-processing of emission inventory data to compile the required IFS input field is carried out before each IFS forecast or analysis cycle. This processing consists of the following steps:

- Grib conversion of netcdf inventory files.
- Mars retrieval of daily biomass burning emissions and injection heights produced by the Global Fire Assimilation System (GFAS).



Table 3.2 *Emission sectors and application of diurnal cycle and injection height range specification.*

Sector	Diurnal Cycle	Injection
Ships (shp)	none	30 - 100 m
Fugitives (fef)	none	surface
Power generation (ene)	sector	200 - 800 m
Off Road transportation (tnr)	none	surface
Road transportation (tro)	sector	surface
Residential and other sectors (res)	sector	surface
Industrial process (ind)	sector	20 - 300 m
Solvents (slv)	sector	surface
Agriculture livestock (agl)	sector	surface
Agriculture soils (ags)	sector	surface
Solid waste and waste water (swd)	none	20 - 100 m
Aviation	none	3D model levels
Biomass burning	sector	daily injection heights maps
Biogenic	species-dependent	surface
Soil and ocean emissions	none	surface
Out-gassing volcanoes	none	2D Map -fixed

- Mapping of species provided in the inventories to the species simulated in the IFS using sectorspecific pre-scaling factors (derived from tuning).
- Spatial interpolation to IFS grid.
- Temporal interpolation to forecast start day from the monthly mean values provide in the inventories (not for biomass burning emissions).
- Capping of grid-point emission values per sector below safety threshold (if applicable).
- Compilation of an emission processing name-list for the IFS.

The processing of the emissions by the IFS is configured by an emission-processing name-list. After the emission files have been read in as part of the initial conditions, the following processing steps are carried out in the IFS at every time step.

- Application of a sector-specific diurnal cycle profile with respect to local solar time.
- Application of specified scaling factors.
- Application of the injection above the surface according to a sector-specific injection height profile
- Aggregation of sector emissions to a single surface flux field per species, that is injected as part of the turbulent tracer diffusion scheme (4.2).

For medium-range forecasts such as the operational 5-day forecasts of reactive gases and aerosols or the 10-day forecast of of greenhouse gases, the daily mean emissions for the first day are also used for all consecutive forecast days. For long-range simulation, there is the option to read in daily emission files at the start of every new simulation day (LMCC_COMPO=true).

(b) Species mapping, scaling factors and emission capping

The specification of the emission processing, i.e. the applied species and sector mappings, the scaling factors and capping values, is contained in a configuration file. The operational configuration for the reactive gases and aerosol for CY48R1 are given in this file: /home/eccams/data/cifs_input/emis_spec/compo_emissions_nrt_48r1_pre.txt.

In this section, we only document some aspects of the external emission processing that leads to a modification of the emissions from the inventory data.



The emission inventories may not contain data for every single species simulated in the IFS. For example, the emissions for volatile organic compounds represented in the COMPO chemistry scheme have to be derived from the groups of volatile organic compounds (VOC) provided in the inventories for anthropogenic, biogenic and biomass burning emissions. An other example of species mapping are the emissions for hydrophilic and hydrophobic organic matter, which are derived from organic carbon emissions and an assumption about the split between the hydrophobic and hydrophilic fractions at the time of the emission release.

The emissions for species in the IFS are constructed from the species or species-groups represented in the emission inventories by using scaling factors during the pre-processing stage as well as inside the IFS. As part of the pre-processing, the emissions for certain IFS species are derived from fractions or linear combination of emissions for the species represented in the inventories. This concerns trace gases and aerosol for which no direct inventory for a given emission type is available, such as certain VOCs, HCN, CH₃CN and OM.

The scaling inside the IFS is applied to split BC and OM emissions in their hydrophilic and hydrophobic components and to approximate emissions for some species based on the CO emissions for certain sectors.

For HCN and CH₃CN we adopt fire emission fluxes based on previous global modelling studies (Singh *et al.*, 2003), in absense of direct GFAS-based estimates. In addition, a small fraction of anthropogenic emissions is included to add up to approx. $0.18 \text{ Tg N yr}^{-1}$ for CH₃CN , and $0.15 \text{ Tg N yr}^{-1}$ for HCN.

For acetone (CH₃COCH₃) a scaling of CO oceanic emissions (20 Tg CO yr^{-1}) to arrive at 28 Tg yr^{-1} is applied.

A further application of the scaling factors inside the IFS is to change the sign of the emission values according to the convention in the IFS. All scaling factors are applied globally in a uniform way for the respective sectors and are not suited to represent any spatial variability of the species-to-species mapping. The IFS scaling factor are configured as part of the emissions specification name-list.

The species to species mapping procedure is often uncertain and can be also be used to modify emissions for a better model performance. For example the conversion factor between OM and OC from the inventory has been optimised based on the model performance and will have to be further reviewed.

Besides the scaling of emissions, the capping emissions flux values above a predefined threshold value is applied for the emissions of OM, BC and SOG2B as part of the pre-processing to avoid excessive mass mixing ratio values. These emission caps are a simple and ad-hoc safety measure and should be reviewed, especially considering that their impact is dependent on the horizontal resolution. The scaling factors are not suited to represent the spatial variability of the species to species relation.

Table 3.3 provides a summary of scaling factors and capping values for selected species.

(c) Application of a diurnal cycle

The diurnal cycle profiles are formulated with respect to solar time, which is 12:00 noon at the time of the highest solar elevation. The solar time definition can deviate up to three hours form the local time because of the time-zones boundaries and daylight-saving time shifts. For the anthropogenic emission sectors, sector specific diurnal profiles are applied. The anthropogenic diurnal profiles (CAMS-GLOB-TEMPO, (Guevara *et al.*, 2021)) were derived from European data sets but are applied globally in the IFS.

The diurnal profile for biomass burning emissions and biogenic VOC emissions is a function f(h) of the local time h defined by 3 parameters: a constant night time value a, the time of local daily maximum b and a measure c for the spread around the time of the local maximum.

$$f(h) = A - \frac{24(1-a)}{C * \sqrt{2\pi}} \exp\left[-0.5\left(\frac{h-b}{c}\right)^2\right]$$
 (3.1)



Table 3.3 *Scaling factors and capping values (Cap) applied to derive emissions of IFS species from the species represented in the emission inventories, selection.*

IFS species	Spliting	Conversion/Tuning	Inventory species	Sectors	Cap [kg/m/s]
SOG2B		0.1	NMVOC	anthropogenic	
OM_A	0.5	1.8	OC	anthropogenic	
OM_B	0.5	1.8	OC	anthropogenic	
BC_A	0.2	1	BC	anthropogenic	
BC_B	0.6	1	BC	anthropogenic	
OM_A	0.5	1.5	OC	Biomass burning	5×10^{-11}
OM_B	0.5	1.5	OC	Biomass burning	5×10^{-11}
BC_A	0.2	1.5	BC	Biomass burning	
BC_B	0.6	1.5	BC	Biomass burning	
CH ₃ COCH ₃		28/20	CO	natural	
HCN		0.001	CO	ene/ind/ref/res	
CH ₃ CN		0.0015	CO	ene/ind/ref/res	
HCN		0.006	CO	Biomass burning	
CH ₃ CN		0.004	CO	Biomass burnng	

For the biogenic emissions the parameters a and b are species-specific to account for different underlying VOC release processes. c is set to a quarter of the local daylight (DL) period. The parameter values were derived from a statistical analysis of the CAMS-GLOB-BIO v1.1 data set. For biomass burning, the parameters are the same as used as in the GFAS code for the calculation of hourly emissions values. The parameters a, b and c for different source groups are listed in 3.4.

Table 3.4 *Parameters of the diurnal profile function: a night time value, b time of local daily maximum and c spread around the time of the local maximum.*

Group	A	В	C	Species
Biomass burning	0.2	13.5	2.0	all
Biogenic VOC_1	0.25	14	DL/4	CH2O, C2H4, ALD2, CH3OH, HCOOH, MCOOH, C2H5OH
Biogenic VOC.2	0.65	14	DL/4	PAR, OLE, C2H6, C3H8, C3H6, C10H16, ISPD, CH3COCH3
Biogenic VOC_3	0.0	14	DL/4	C5H8

(d) Injection of elevated emissions

Elevated emissions (Table 3.2) are directly converted into tendencies of mass mixing ratios (C) at each model time step. The injection is carried out uniformly w.r.t to pressure in a vertical injection range defined by a lower and upper model level k_{\min} and k_{\max} . The resulting tendency of C at each model level k is calculated from the 2D emission flux E in the following way:

$$\frac{\partial C_k}{\partial t} = ff_k \times E \times \frac{G}{\Delta p_k} \text{ with } ff_k = \frac{\Delta p_k}{\sum\limits_{k=k_{\min}}^{k_{\max}} \Delta p_k} \text{ for } k_{\min} \le k \le k_{\max}$$
(3.2)

The injection height profile ranges ($k_{min} \le k \le k_{max}$) are configured based on:

- Upper and lower injection heights (anthropogenic sectors, see Table 3.2) or
- Gridded map of injections heights with a specified number of model levels below and above (volcanic emission and biomass burning emissions).

Alternatively to the injection range specification, a 3D set of model level fields containing the emissions fluxes (units kg/m/s) for each model level can be read in by the IFS. This approach is used for aviation emissions of CO_2 and NO_x



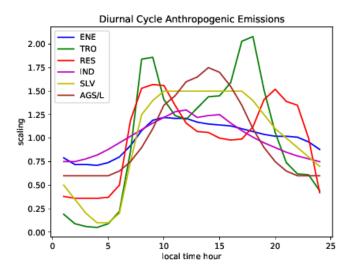


Figure 3.1 Diurnal profile of anthropogenic emission sectors with respect to local solar time (CAMS-GLOB-TEMPO)

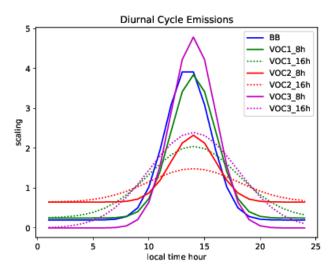


Figure 3.2 Diurnal profile of biomass burning and biogenic VOC emissions for a 8 h and 16 h daylight period.

Surface emissions are injected in the atmosphere by means of the turbulent diffusion scheme. The emissions are combined with the dry deposition fluxes to surface flux that is used as lower boundary condition for the vertical turbulent tracer diffusion scheme (Part IV Physical processes, Chapter 3.7).

3.1.2 On-line emissions of desert dust and sea salt

(a) Emissions of desert dust

The dust emission of CY48R1 combines the approaches of Marticorena and Bergametti (1995) for the representation of the saltation process and of Kok (2011) for the size distribution of desert dust emissions. This new dust scheme was adapted from the scheme implemented in TACTIC (Michou *et al.*, 2015; Nabat *et al.*, 2012).



The emissions of dust particles of a given size D_p through sandblasting occurs if the friction velocity u^* is above a threshold value $u_t^*(D_p)$, written as

$$u_t^*(D_p) = u_{ts}^*(D_p) f_{eff} f_w,$$
 (3.3)

where $u_t^* s(D_p)$ represents an minimum threshold friction velocity and is determined according to the parameterization of Marticorena and Bergametti (1995) as a function of the Reynolds number R_e as

$$u_{ts}^{*}(D_{p}) = 0.129 \times K \times \begin{cases} [1 - 0.858 \times exp(-0.0617(R_{e} - 10))] & R_{e} > 10\\ (1.928 \times R_{e}^{0.092} - 1)^{-0.5} & R_{e} \le 10 \end{cases}$$
(3.4)

Here, the Reynolds number R_e is parameterized following (Marticorena and Bergametti, 1995) as

$$R_e = 1331.647 \times D_p^{1.561228} + 0.38194 \tag{3.5}$$

and

$$K = \sqrt{\frac{2 \times g \times \rho_p \times D_p}{\rho_a} \times \left[1 + \frac{0.006}{\rho_g \times g \times (2 \times D_p)^{2.5}}\right]}$$
(3.6)

Where D_p is the particle diameter in cm, ρ_p is the dust aggregate density taken as 2.6 kg/m^3 , ρ_a is the surface air density and g the gravitational constant. It should be noted that the 1331.647 factor has a unit of cm^{-1.561228} to make sure that R_e is dimensionless. Similarly, the 0.006 factor has a unit of $g/cm^{0.5}s^{-2}$. All other factors are unitless. The term f_{eff} is a correction factor accounting for the effect of surface roughness, expressed as:

$$f_{eff} = 1 - \left[\frac{ln\left(\frac{z_m}{z_{0s}}\right)}{ln\left(0.35\left(\frac{10}{z_{0s}}\right)^{0.8}\right)} \right]$$
(3.7)

Where z_m is the aerodynamic roughness length and z_{0s} is the roughness length of smooth erodible surfaces, both in m. Finally, f_w accounts for the effect of soil moisture content on the threshold friction velocity. Following Fecan *et al.* (1999), it is parameterized as:

$$f_w = \begin{cases} [1 + 1.21 \times (w - w')^{0.68}]^{0.5} & \text{for } w > w' \\ 1 & \text{for } w < w' \end{cases}$$
(3.8)

Where w is the surface soil moisture, provided by the IFS surface scheme, and w' is a threshold gravimetric water content of the top soil layer above which w increases the threshold friction velocity u_t^* , expressed as:

$$w' = 0.0014 \times (\%clay)^2 + 0.17 \times (\%clay)$$
(3.9)

Where %clay is the fraction of soil that is composed of clay. Both w and w' are in percent. The information on the clay, silt and sand fraction is provided externally by the Global Soil Data set for use in Earth system models (GSDE, (Shangguan *et al.*, 2014). The horizontal flux of dust from saltation is expressed as:

$$G(D_p) = E_{soil} \times \frac{\rho_a}{g} \times S_{rel}(D_p) \times (u^*)^3 * \left(1 - \left(\frac{u_t^*(D_p)}{u^*}\right)^2\right) \times \left(1 + \frac{u_t^*(D_p)}{u^*}\right)$$
(3.10)

Where E_{soil} is the soil "erodibility" and S_{rel} is the ratio of the surface of the dust aggregate of diameter D_p over the sum of the surface of aggregates of all diameters. Both are unitless. The soil erodibility can be defined as the soil erosion efficiency of a surface under a given meteorological forcing (Zender *et al.*, 2003). It is also often denoted as "dust source function". Because soil erodibility is hard to estimate, several methods have been tested in dust emission schemes, one of the most commonly used is the topographic approach from Ginoux *et al.* (2001), which assumes that the topographic depressions are the largest source of dust. In cyle 47R1, the soil erodibility/dust source function (DSF) is provided



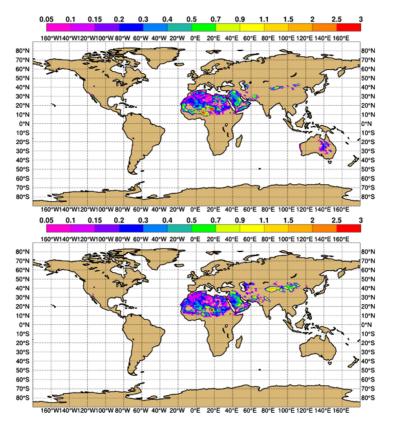


Figure 3.3 Dust source function (DSF) used in CY48R1 for January (top) and May (bottom)

empirically by a climatological dataset of the frequency of occurrence of dust AOD > 0.4, as provided by Paul Ginoux and introduced in Ginoux *et al.* (2012). In cycle 46R1, the climatological frequency of dust AOD > 0.2 was used for the DSF, which led to an overestimation of simulated dust AOD. In cycle 48R1, the DSF has been recomputed by comparing daily dust AOD from a simulation and provided by the MIDAS product (Gkikas *et al.*, 2020) over a three years period. Using a longer period of time to recompute the DFS allowed for the provision of a monthly DSF, instead of a fixed (yearly) one used from cycles 46R1 to 47R3. The DSF for January and May is shown in Figure 3.3. There are significant differences between the two, such as higher values over the Sahel in January, possibly partly over cultivated areas (Ginoux *et al.*, 2012), and over Australia, and higher values over the Taklimakan in May.

The friction velocity u^* is computed using as an input the 10m wind speed that includes a gustiness effect, computed as in Rémy *et al.* (2019). Finally, the flux of vertically emitted dust is computed from the horizontal flux using Gilette (1979):

$$H(D_p) = G(D_p) \times F_{bare} \times C \times \begin{cases} 10^{0.134 \times (\%clay) - 6.0)} & \text{for } \%clay \le 17\% \\ 10^{-0.09 \times (\%clay) - 2.19)} & \text{for } \%clay > 17\% \end{cases}$$
(3.11)

where F_{bare} is the fraction of the soil that is bare; C is a normalization constant set to 0.034, nearly similar to the value used in Nabat *et al.* (2012) who used 0.035. This formula is integrated for all particle diameters D_p and provides the total flux of emitted dust. In order to distribute this flux into the three bins, the size distribution at emissions of Kok (2011) is used, which means a much larger share of emissions being distributed to the super coarse bin as compared to the Ginoux *et al.* (2001) scheme used operationally before cycle 46R1. This is illustrated by Table 3.5, and as a consequence the simulated lifetime of total dust is significantly lower with the new scheme as compared to the old scheme, because the super coarse dust bin has a much shorter lifetime from increased dry deposition and sedimentation.



A new development has been implemented into cycle 48R1 (activated if the swith LAERDUSTSIZEVAR is set to true, which is the case by default in cycle 48R1) whereby the distribution of the total dust emissions into the three bins is modulated regionally using an external file, which provides the fraction of total emissions that goes into bin1 and bin2. This fraction has been computed using long simulations of dust mineralogy (the dust mineralogical species being emitted preferentially to bin1 and 2 or bin3). This results on average on slightly more emissions being distributed to bin1 and 2 as compared to cycle 47R3.

Table 3.5 also shows the impact of the new optical properties and of the new DSF implemented in cycle 48R1: less extinctive dust leads to higher dust emissions (for a global dust AOD roughly unchanged) and burden in cycle 48R1 as compared to cycle 47R3. Also, the distribution of the total dust emissions between the three bins is slightly changed in cycle 48R1, with relatively slightly more emissions to bins 1 and 2 as compared to bin 3, coming from the regional modulation of the dust size distribution at emissions implemented in cycle 48R1.

Table 3.5 Desert dust emissions, burden and lifetime simulated by IFS-AER cycles 45R1, 47R1, 47R3 and 48R1 (forecast only). The emissions are in Tg yr^{-1} , the burdens are in Tg and the lifetimes are in days.

process	bin1 (0.05 - 0.55 μm)	bin2 (0.55 - 0.9 μm)	bin3 (0.9 - 20 μm)	total
Emissions (45R1)	87.9	292	2054.9	2434.8
Burden (45R1)	1.7	5.9	8.5	16.1
Lifetime (45R1)	7.0	7.2	1.5	2.4
Emissions (47R1)	4.9	45.2	3248.5	3298
Burden (47R1)	0.12	1.0	13.5	14.6
Lifetime (47R1)	8.9	8.1	1.5	1.6
Emissions (47R3)	5.1	47.8	3456.5	3509.4
Burden (47R3)	0.12	1.1	16.4	17.62
Lifetime (47R3)	8.6	8.4	1.7	1.8
Emissions (48R1)	11.1	103.3	5537.1	5651.4
Burden (48R1)	0.26	2.4	27.2	29.86
Lifetime (48R1)	8.5	8.5	1.8	1.9

(b) Emissions of sea salt

In addition to the M86 (Monahan *et al.*, 1986) and the G14 (Grythe *et al.*, 2014) sea salt aerosol emission schemes used in previous cycles, a new sea salt emission scheme "A16" based on Albert *et al.* (2016) has been developed and is used operationally since cycle 47R1. It is similar to the M86 scheme in the sense that as a prerequisite, the oceanic whitecap fraction is first estimated; in the M86 scheme this is done following the work of Monahan and Muircheartaigh (1980). In the A16 scheme, this is done by a statistical fit between a dataset of one year of whitecap fraction estimated from remote sensing observations of ocean surface brightness by radiometers onboard the WindSat satellite, at two frequencies: 10 and 37 GHz (Anguelova and Webster, 2006), and 10m wind speed provided by Quickscat as well as sea-surface temperature provided by ERA interim. The whitecap fraction W is expressed as a function of 10m windspeed U_{10} and SST by:

$$W = a(SST) [U_{10} + b(SST)]^{2}$$
(3.12)

where

$$a(SST) = a_0 + a_1 SST + a_2 SST^2 (3.13)$$

$$b(SST) = b_0 + b_1 SST \tag{3.14}$$

The $a_{0,1,2}$ and $b_{0,1}$ parameters are given in Albert *et al.* (2016) for the whitecap fraction estimated with WindSat 10 and 37 GHz brightness temperature. As the coverage of the retrieved whitecap fraction data set is very good, the sample size is very large, which makes the fit quite robust. In the IFS-AER implementation of this scheme, using the fit to whitecap from 37 GHz brightness temperature gave better results, and the $a_{0,1,2}$ and $b_{0,1}$ parameters for this wavelength were chosen.



Using the oceanic whitecap fraction as an input, the production flux of sea salt aerosol is then computed by the following formula from Monahan *et al.* (1986):

$$\frac{dF}{D_p} = 3.610^5 W D_p^{-3} (1 + 0.057 D_p^{1.05}) 10^{1.19 \exp(-B^2)}$$
(3.15)

where

$$B = \frac{0.38 - \log(D_p)}{0.65} \tag{3.16}$$

and D_p is the particle diameter.

Table 3.6 shows the simulated emissions, burden and lifetime of the three sea salt bins for the three available emission schemes. The lifetime of sea-salt aerosol decreases for larger particles, because sedimentation, applied only to bin 3, is an effective sink, and because the simulated dry deposition velocity increases with particle size for particles above 1 micron diameter. The emissions of super coarse sea salt aerosol are much higher with the G14 scheme as compared to the two others. Similar to the M86 scheme, the A16 scheme shows a relatively smaller increase in emissions with bin size. The lifetime of coarse and super coarse sea salt bins is the lowest with the A16 scheme. The M86 scheme has been used operationally until cycle 43R3. The G14 scheme has been used operationally in cycles 45R1 and 46R1, while the new A16 scheme has been implemented in operational CY47R1 IFS-AER. More detail on the A16 scheme can be found in (Remy and Anguelova, 2021).

Table 3.6 Dry sea salt aerosol emissions, burden and lifetime simulated by IFS-AER with the M86, G14 and A16 schemes. The emissions are in $Tg yr^{-1}$, the burdens are in Tg and the lifetimes are in days.

process	bin1 (0.05 - 0.5 μm)	bin2 (0.5 - 5 μm)	bin3 (5 - 20 μm)	total
Emissions (up to 43R3,M86)	32.2	2767.2	3363.8	6163.2
Burden (up to 43R3,M86)	0.09	3.53	1.43	5.05
Lifetime (up to 43R3,M86)	1.0	0.46	0.16	0.29
Emissions (45R1-46R1,G14)	41.6	1799.5	45531.6	47372.7
Burden (45R1-46R1,G14)	0.14	2.86	22.5	25.5
Lifetime (45R1-46R1,G14)	1.3	0.58	0.18	0.2
Emissions (from 47R1,A16)	110.3	6595.5	13657.8	20363.6
Burden (from 47R1,A16)	0.39	4.46	1.41	6.2
Lifetime (from 47R1,A16)	1.3	0.25	0.04	0.11

3.1.3 Lightning as source of Nitrogen Oxides

NO production from lightning is a considerable contribution to the global atmospheric NOx budget. Estimates of the global annual source vary between 2 and 8 Tg N yr⁻¹ (Schumann and Huntrieser, 2007). 5 Tg N yr⁻¹ is the most commonly assumed value for global CTMs, which is about 6–7 times the value of NO emissions from aircraft (Gauss *et al.*, 2006), or about one fifth of the total anthropogenic NO emissions. NO emissions from lightning play an important role in the chemistry of the atmosphere because they are released in the rather clean air of the free troposphere. The parameterisation of the lightning NO production in IFS consists of estimates of

- the flash rate density,
- the flash energy release and
- the vertical NO emission profile for each model grid column.

The IFS includes several paramaterisations to diagnose the flash rate density using input parameters from the convective scheme. For the simulation of the lightning NO emissions, the flash-rate density is estimated to be proportional to the convective rain-flux at the surface (Meijer *et al.*, 2001) using a conversion factor of 1728 over land and 172.8 over ocean. Further, lightning occurrences are only computed if the cloud base height is below 4 km, the cloud top height above 5 km and the temperature profile reaches values below -25°C. The energy produced by each flash and the associated NO release is calculated using a global conversion factor for the energy and the released number of NO molecules



per energy unit. The combined factor is further multiplied with an empirical tuning factor to ensure that the total annual lightning emissions are equal to 5 Tg N. The tuning factor is resolution dependent and compensates modifications to the convective activity introduced by upgrades of the model physics. It is determined by a 1-year test simulation. The vertical distribution of the NO lightning emissions adopts a "backward C-shape" profile (Ott *et al.*, 2010), which locates most of the emission in the middle of the troposphere (Fig. 3.4) As lightning NO emissions occur mostly in situations with strong convective transport, tests showed that differences in the injection profile had little impact.

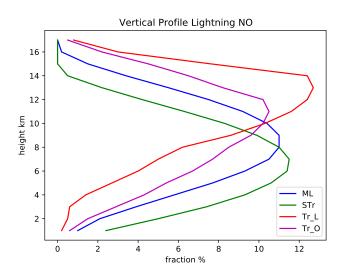


Figure 3.4 *Vertical Profile of the Lightning NO production (fraction in % for Mid-latitudes (ML), Subtropics (STr), Tropics over land (Tr_L) and Tropics over Oceans (Tr_O).*

3.1.4 CO₂ biogenic fluxes

The total CO₂ biogenic flux over land ecosystems is represented by the Net Ecosystem Exchange (NEE). NEE is composed of the sum of two fluxes with opposite sign: the Gross Primary Production (GPP) flux associated with the CO₂ sink from plant photosynthesis and the ecosystem respiration (R_{eco}) corresponding to the CO_2 emissions from autotrophic and heterotrophic ecosystem respiration. Both GPP and R_{eco} are modelled online in the IFS Land Surface Scheme (Part IV Physical processes, Chapter 8). In cycle 48R1, the Farquhar et al. (1980) photosynthesis parametrization is used to model GPP, while previous cycles used the A-gs photosynthesis scheme (Boussetta et al., 2013). A detailed description of the photosynthesis model is available in Part IV Physical processes, Chapter 8, section 8.7.2 for CY48R1 and Part IV Physical processes, Chapter 8, section 8.7.1 for previous cycles. The ecosystem respiration R_{eco} is the sum of two fluxes: autotrophic dark respiration R_d , which is modelled within the photosynthesis module, and R_{soilstr} encompassing both heterotrophic respiration from the soil and autotrophic respiration from the above and below ground structural biomass. Rsoilstr is parametrized using an empirical equation with a plant-functional-type (PFT) dependent reference ecosystem respiration constant together with three functions which represent the temperature, soil moisture and snow cover dependencies, as documented in Part IV Physical processes, Chapter 8, section 8.7.3. The sign of both GPP and Reco follows the IFS Land Surface Scheme convention, which means that GPP is always positive and R_{eco} is negative.

The coupling of the NEE flux to the atmospheric CO_2 forecast is enabled by the flag LNEEONLINE which is set to True by default. Modelling the NEE online has the benefit of having consistent temporal and spatial resolution with the transport model, but it can also result in large-scale biases (Agustí-Panareda *et al.*, 2014). Thus, the NEE needs to be bias corrected in order to avoid any large-scale biases in NEE leading to drifts in the atmospheric CO_2 forecast. The Biogenic Adjustment Flux Scheme (BFAS) provides an online PFT-dependent bias correction to NEE by correcting either R_{eco} , GPP or both. In cycle 48R1, only the modelled R_{eco} component is corrected, as it is deemed to have the largest uncertainty. In



earlier cycles, the strategy was to correct the dominant flux, e.g. R_{eco} in the winter and GPP during the growing season. A detailed description of BFAS can be found in Agustí-Panareda *et al.* (2016).

3.1.5 Code overview

The processing of the emission inventory input is done in the routine COMPO_APPLY_EMISSIONS. It calls the routine APPLY_EMISSIONS_2D, which loops over the emissions specification structure YEMIS2D_DESC. The structure (part of namelist NAMCOMPO_EMIS) defines the target species, sectors ,scaling factors, choice of diurnal cycle profile and injection height method. The emission fields are multiplied with the local diurnal cycle factor,calculated in COMPO_DIURNAL and further scaling factors before they are added to the tracer-specific surface flux if the emissions are configured as surface emissions in YEMIS2D_DESC. The surface flux is input to the vertical tracer diffusion scheme (VDFDIFC). When the application of a injection profile method is configured in YEMIS2D_DESC, the emission field is converted to a vertical profile of MMR tendencies, which are added to the tracer tendencies in APPLY_EMISSIONS_2D. Aviation emissions are read in as 3D model level fields and are added to the tracer tendencies in APPLY_EMISSIONS_3D.

The sea salt emissions are calculated in AER_SSALT_ALBERT, which is called in the following sequence: AERINI_LAYER, AER_PHY2 and AER_SRC. The desert dust emissions are calculated in AER_SRC.

CULINOX is the routine, which computes the NO emissions from lightning based on the flash densities provided by the lightning code of the IFS.

The CO₂ fluxes are calculated by the COTWORESTRESS and SRFCOTWO modules in the land surface scheme (Part IV Physical processes, Chapter 8). The photosynthesis model is in routine FARQUHAR which is called by COTWORESTRESS, and COTWORESTRESS is called by VSURF. The ecosystem respiration is calculated by SRFCOTWO. Both VSURF and SRFCOTWO are called by the interface routine of the land surface model (SURFEXCDRIVER).

3.2 REMOVAL BY DEPOSITION

3.2.1 Dry deposition

Dry deposition is a major removal pathway for many reactive gases and aerosols, which removes the tracers from the atmosphere by either sticking to or reacting with the surface or vegetation. The spatial and temporal variability of dry deposition is controlled by turbulent mixing and by surface properties.

Solubility and reactivity are properties that determine the effectiveness of dry deposition for the chemical species. Ozone is a prototype for a very reactive and insoluble species and SO_2 is the prototype for a soluble species. The effectiveness of the dry deposition of aerosols is governed by their size and shape, i.e their aerodynamic properties and whether they are heavy enough to be subject to gravitational sedimentation. Dry deposition is a highly uncertain process and deposition fluxes are difficult to measure. Modelling of dry deposition is based on empirically determined parameters (reference resistances) that are provided for different land use and vegetation classes and prototypes for reactive and soluble species.

(a) Dry deposition for reactive gases

The deposition dry flux (Φ_D) is approximated using a dry deposition velocity (V_D) that describes the effectiveness of the dry deposition process and the MMR at the lowest model level C.

$$\Phi = -\rho V_D C \tag{3.17}$$

 V_D is modelled following a "big-leaf" approach introduced by Wesely (1989). Fig. 3.5 shows the parallel and serial pathways assumed for the dry deposition modelling in the IFS. The "big-leaf" approach treats the canopy as one entity without vertical structure. The dry deposition velocity is simulated based on a combination of resistances, namely the aerodynamic resistance r_a , the quasi-laminar sub-layer resistance r_b and the canopy/surface resistance r_c in the following way:



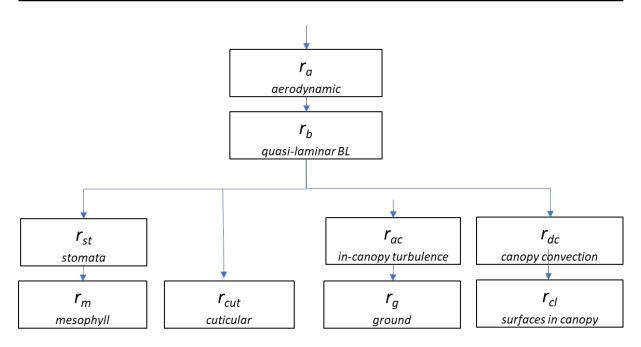


Figure 3.5 Schematic of the components of the "big-leaf" resistance approach following Wesely (1989) applied in the IFS. The resistance terms are: aerodynamic resistance (r_a) , resistance to the quasi-laminar boundary layer around the bulk surface (r_b) , stomatal resistance (r_{st}) , mesophyll resistance (r_m) , cuticular resistance (r_{cut}) , resistance associated with within-canopy convection (r_{dc}) , resistances to surfaces in the lower canopy (r_{cl}) , resistance to in-canopy turbulence (r_{ac}) and resistance at the ground (r_g)

.

$$V_D = \frac{1}{r_a + r_b + r_c} \tag{3.18}$$

 r_a is simulated under the surface layer assumptions outlined in Part IV Physical processes, Chapter 3, Section2 r_a [s m⁻¹] is derived from the bulk transfer coefficient for tracer mass C_c (dimensionless) and the surface wind speed U_n (Part IV Physical processes, Eq. 3.19)

$$r_a = \frac{1}{C_c U_n} \tag{3.19}$$

 C_c is formulated in an equivalent as the transfer coefficients for moment, heat and moisture (C_M , C_H , C_Q , (Part IV Physical processes, Eq. 3.16-18)) based on the stability function for heat and moisture considering stable and unstable situations using Monin-Obuchov similarity theory. While the transfer coefficients are calculated over all tile fraction in the grid box, only the value from the dominate tile is used for the dry deposition calculations.

The quasi-laminar boundary layer resistance around the bulk surface (r_b , [s m⁻¹]) follows Wesely and Hicks (1977):

$$r_b = \frac{2}{ku_*} \left(\frac{\kappa}{D_A}\right)^{\frac{2}{3}} \tag{3.20}$$

The parameter $\kappa = 2.0 \times 10^{-5}$ [m² s⁻¹] is the thermal diffusivity of air; D_X [m² s⁻¹] is the diffusivity of gas X in air. k is the von Kármán constant and u^* the friction velocity calculated from the IFS land surface scheme (Part IV Physical processes, Chapter 8).

The components of the bulk surface resistance (r_c) depend on the underlying surface and vegetation properties. Hence, the deposition velocities are calculated for each surface tile fraction separately and a resulting dry deposition velocity is constructed from the weighted mean of tile fractions. r_c is composed



of different pathways of interaction of the deposited gases with the surface, the canopy, the cuticle of plant and its uptake via the stomata. For vegetated surfaces, r_c is calculated from a combination of series and parallel resistances:

$$r_c = \left(\frac{1}{r_{st} + r_m} + \frac{1}{r_{cut}} + \frac{1}{r_{dc} + r_{cl}} + \frac{1}{r_{ac} + r_g}\right)^{-1}$$
(3.21)

 $r_s t$ is the stomatal resistance, r_m is the mesophylic resistance, r_{cut} is the cuticular resistance, r_{dc} is the resistance associated with within-canopy convection, r_{cl} is the resistance to surface removal in the lower canopy, r_{ac} is the resistance to in-canopy turbulence, and r_g is the ground resistance.

For non-vegetated surface tiles such bare ground, ice, snow-covered vegetation, ocean and lake the canopy related terms are neglected resulting in $r_c = r_g$. The bulk surface resistance for the highly soluble gases HNO_3 and H_2O_2 is set to a fixed value of $r_c = 10$ s m⁻¹ independent of the land cover and vegetation type of the surface, which means an efficient dry deposition if that is not limited by the aerodynamic or quasi-laminar boundary layer resistance.

In particular, the variability of stomatal uptake is simulated depending on the meteorological conditions.

The numerical values of the reference resistances parameters are taken from the GEOS-Chem model and are listed in table 3.7. The mapping of the IFS land use tiles and vegetation types to the GEOS-Chem land use type is listed in 3.8

The IFS applies currently a stomatal resistance (r_{st}) calculation for dry deposition following Wang *et al.* (1998) that has been pulled from the GEOS-Chem model.

$$r_{st} = \frac{D_w}{D_X} \frac{r_i}{LAI_{eff}f(T_a)}$$
(3.22)

The parameter r_i is the initial stomatal resistance that is tabulated for the GEOS-Chem 3.7; D_w [m² s⁻¹] is the diffusivity of water vapor or tracer X in air. It should be noted that the diffusivities are uncertain values. Usually, the diffusivity ratio for O_3 is assumed to has the value of 1.6 whereas the choice of the parameter values in GEOS-Chem results in a diffusivity ratio value of 1.3 leading to smaller stomatal resistance. LAI_{eff} [m² m⁻²] is effective leaf area of actively transpiring leaves. The variable LAI_{eff} is calculated with a function (called 'biofit' in the source code) from leaf area index (LAI), solar zenith angle and cloud fraction. When incident shortwave radiation is zero (i.e. at night), LAI_{eff} is set to 0.01 m² m⁻². The function was fitted to match the results of a multi-layer canopy radiative transfer model. The function describing the impact of air temperature (T_a , [°C]) is given by:

$$f(T_a) = T_a \frac{40 - T_a}{400} \tag{3.23}$$

The mesophyll resistance (r_m , [s m⁻¹]) is given by:

$$r_m = \left(\frac{H}{3000} + 100f_0\right)^{-1} \tag{3.24}$$

The variable H is the Henry's law constant of the species which varies with air temperature [0.01 M atm⁻¹ at 298 K for ozone]. f_0 is the reactivity factor, which expresses the tendency to chemically react with respect to the reactivity to ozone. $f_0 = 1$ is the value for ozone and H_2O_2 , $f_0 = 0.3$ for CH_2OOH and $f_0 = 0.1$ for selected nitrogen species and hydrocarbons. $f_0 = 0$ is the value for all other species, which means that only their solubility, expressed by H, determines the effectiveness of their dry deposition.

The resistance associated with in-canopy convection (r_{dc}) follows:

$$r_{dc} = 100 \left(1 + \frac{1}{G} \right) \tag{3.25}$$



The variable G [W m⁻²] is the incoming shortwave radiation.

Cuticular resistance (r_{cut}) is given by:

$$r_{cut} = \frac{r_{lu}}{LAI} \left(\frac{H}{10^5} + f_0 \right)^{-1} \tag{3.26}$$

The parameter r_{lu} is the initial resistance for cuticular uptake.

The resistances to surfaces in the lower canopy (r_{cl}) and the ground (r_g) are calculated using a similar structure consisting of processes related to solubility and reactivity using SO₂ (subscript S) and ozone (subscript O) as reference species. Specifically, the ground resitances is given by:

$$r_g = \left(\frac{H}{10^5} \frac{1}{r_{S,g}} + \frac{f_0}{r_{O,g}}\right)^{-1} \tag{3.27}$$

and the resistances to surface in the canopy:

$$r_{cl} = \left(\frac{H}{10^5} \frac{1}{r_{S,cl}} + \frac{f_0}{r_{O,cl}}\right)^{-1} \tag{3.28}$$

The resistance because of in-canopy turbulence r_{ac} is a land-use specific value (3.7).

To consider the effects of air temperature (T_a) a resistance term $r + T = 1000 \exp(-T_a - 4 - 273)$ is added to to the tabulated resistance parameters r_{lu} , $r_{S,g}$, $r_{O,g}$, $r_{S,cl}$ and $r_{O,cl}$.

Table 3.7 Reference resistances used for the dry deposition of gases based on GEOS-Chem land types. R_i : the minimal stomatal resistances (differs from values used in IFS Land Surface Scheme), R_{lu} : the uptake pathway for leaf cuticles, R_{ac} : resistances within the canopy, $R_{gs,O}$: uptake pathways for the ground including soil, leaf litter for O_3 . $R_{cl,o}$: the uptake pathways by in the lower canopy by leaves, twigs, bark etc. for O_3 .

GC	Snow	Deciduous	Conifer	Agricultural	Shrub	Amazon	Tundra	Desert	Wetland	Urban	Water
	Ice	Forest	Forest	Land	Grassland	Forest					
$\overline{R_i}$		200	400	200	200	200	200		200		
R_{lu}		9000	9000	9000	9000	1000	4000		9000		
R_{ac}	0	2000	2000	200	100	2000	0	0	300	100	0
$R_{gs,O}$		200	200	150	200	200	340	400	1000	300	2000
$R_{cl,O}$	1000	1000	1000	1000	1000				1000		

(b) Dry deposition for aerosols

A new parameterization of aerosol dry deposition following Zhang and He (2014) has been implemented in cycle 47R1 IFS-AER and is used operationally since CY47R3. The Zhang and He (2014) has been implemented because it gave good results in a recent inter-comparison of dry deposition schemes (Khan and Perlinger, 2017), and also because instead of use the particle size as an input, it divides particles in size ranges: fine, coarse and giant (super-coarse). Only the surface resistance differs as compared to the Zhang *et al.* (2001) scheme. The inverse of the surface resistance is also referred to as surface deposition velocity and denoted as V_D . It is computed as as a function of the particle diameter D_p and friction velocity u^* as:

$$V_{D} = \begin{cases} a_{1} \times u_{*} & \text{for } D_{p} \leq 2.5 \mu m \\ \left(b_{1} \times u_{*} + b_{2} \times u_{*}^{2} + b_{3} \times u_{*}^{3}\right) \times \exp\left(K_{1} \times \left(\frac{LAI}{LAI_{MAX}} - 1\right)\right) & \text{for } 2.5 \mu m < D_{p} \leq 10 \mu m \\ \left(d_{1} \times u_{*} + d_{2} \times u_{*}^{2} + d_{3} \times u_{*}^{3}\right) \times \exp\left(K_{2} \times \left(\frac{LAI}{LAI_{MAX}} - 1\right)\right) & \text{for } D_{p} > 10 \mu m \end{cases}$$
(3.29)

Where



IFS Vegetation Type	IFS tile	GEOS-Chem Type
Crops, Mixed Farming	Low vegetation	Agricultural
Short Grass	Low vegetation	Shrub/Grassland
Evergreen Needleleaf Trees	High vegetation	Coniferous Forest
Deciduous Needleleaf Trees	High vegetation	Coniferous Forest
Deciduous Broadleaf Trees	High vegetation	Deciduous Forest
Evergreen Broadleaf Trees	High vegetation	Amazon
Tall Grass	Low vegetation	Shrub/Grassland
Desert	Low vegetation	Desert
Tundra	Low vegetation	Tundra
Irrigated Crops	Low vegetation	Agricultural
Semidesert	Barren ground	Desert
Ice Caps and Glaciers	Ice	Snow/Ice
Bogs and Marshes	Low vegetation	Wetland
Inland Water	Water	Water
Ocean	Ocean	Water
Evergreen Shrubs	Low vegetation	Shrub/Grassland
Deciduous Shrubs	Low vegetation	Shrub/Grassland
Mixed Forest/Woodland	High vegetation	Deciduous Forest
Interrupted Forest	High vegetation	Deciduous Forest
Water and Land Mixtures	Water	Wetland
Lake	Lake	Water
Urban		Urban, if implemented
	Snow on vocatation	Spow /Ico

Table 3.8 Mapping of IFS vegetation and land use classes to GEOS-Chem Land use types

Snow on vegetation Snow/Ice

$$K_1 = c_1 \times u_* + c_2 \times u_*^2 + c_3 \times u_*^3$$

 $K_2 = e_1 \times u_* + e_2 \times u_*^2 + e_3 \times u_*^3$

Where a_i , b_i , c_i , d_i , e_i are land-surface dependent coefficients are provided in Tables 2a and 2b of Zhang and He (2014). LAI_{MAX} is the maximum leaf area index for a given land surface category, which has been estimated from the LAI climatology used in the IFS. Figure 3.6 shows a comparison of the simulated dry deposition velocity by the Zhang *et al.* (2001) and Zhang and He (2014) schemes over a particular land surface category (desert).

In cycle 48R1, a parameterization of the rebound effect of super-coarse dust particles over oceanic surfaces has been, implemented following Zhang *et al.* (2001). The surface resistance for super coarse dust particles, as parameterized in the Zhang and He (2014) scheme, is multiplied by a factor R over non-water surfaces, if the friction velocity is above 0.335 m s⁻¹, following results from field campaigns as detailed in Bergametti *et al.* (2018):

$$R = \exp\left(R_0 S_t^{1/2}\right) \tag{3.30}$$

Where R_0 is a constant set to 0.1 and S_t is the Stokes number. Following Zhang *et al.* (2001), S_t is computed differently between vegetated surfaces and smooth surfaces (or surfaces with bluff roughness elements):

$$S_t = V_D u^* / gA$$
 over vegetated surfaces (3.31)

$$S_t = V_D u^{*2} / \mu$$
 over smooth surfaces (3.32)

Where A is the characteristic radius of collectors (provided in Table 3 of Zhang *et al.* (2001), g is the gravity constant, μ is the kinematic velocity of air and V_s is the gravitational settling velocity computed



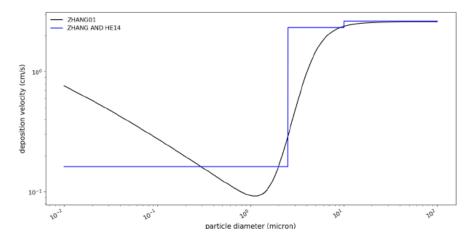


Figure 3.6 Dry deposition velocity with a friction velocity of 1 m/s, over a desert surface as a function of particle size, parameterized by the Zhang et al. (2001) and the Zhang and He (2014) schemes.

as a function of particle radius r and density ρ_v . C_F is the Cunningham correction factor.

$$V_{\rm s} = \frac{2\rho_{\rm p}g}{9\mu} \, r^2 \, C_{\rm F} \tag{3.33}$$

3.2.2 Wet deposition

Wet deposition is the transport and removal of soluble or scavenged trace gases and aerosol by precipitation. It includes the following processes:

- In-cloud scavenging and removal by rain and snow (rain-out).
- Release by evaporation of rain and snow.
- Below-cloud scavenging by precipitation falling through without formation of precipitation (wash-out).

It is important to take the sub-grid scale of cloud and precipitation formation into account for the simulation of wet deposition. The IFS cloud scheme provides information on the cloud and the precipitation fraction for each grid box. It uses a random overlap assumption (Jakob and Klein, 2000) to derive cloud and precipitation area fraction. The precipitation fluxes for the simulation of wet removal in IFS are divided by the precipitation fraction of the grid cell in order to be valid over the precipitation fraction of the respective grid box.

The loss of trace gas and aerosol by rain-out and wash-out is limited to the area of the grid box covered by precipitation. Likewise, the cloud water and ice content is scaled to the respective cloud area fraction.

If the sub-grid-scale distribution was not considered in this way, wet deposition would be lower for highly soluble species such as HNO_3 and aerosol because the species is only removed from the cloudy or rainy grid box fraction.

Even if wet deposition removes tracer mass only in the precipitation area, the mass mixing ratio representing the entire grid box is currently changed accordingly after each model time step. This is equivalent to the assumption that there is instantaneous mixing within the grid box on the timescale of the model time step.

The module for wet deposition in IFS is based on the Harvard wet deposition scheme (Jacob *et al.*, 2000; Liu *et al.*, 2001) with additions derived from Luo *et al.* (2019). The input fields to the wet deposition routine are the following prognostic variables, calculated by the IFS cloud scheme (Forbes *et al.*, 2011): total cloud and ice water content, grid-scale rain and snow water content and cloud and grid-scale precipitation fraction as well as the derived fluxes for convective and grid-scale precipitation fluxes at



the grid cell interfaces. For convective precipitation, a precipitation fraction of 0.05 is assumed and the convective rain and snow water content is calculated using the convective liquid precipitation rate and assuming a droplet fall speed of 5 m s^{-1} .

All aerosols and the following soluable chemical species are subject to wet deposition: O3, H2O2, CO, HNO3, CH3OOH, CH2O, NO, HO2, CH3O2, NO2, N2O5, HO2NO2, NO3, HCL, CLONO2, HOCL, HBR, BRONO2, HOBR, ALD2, PAN, ROOH, ONIT, C5H8, SO2, NH3, SO4, NH4, MSA, CH3COCHO, Pb, CH3OH, HCOOH, MCOOH, C2H6, C2H5OH, ISPD, CH3COCH3, HONO, HCN, CH3CN, XYL, TOL, HPALD1, HPALD2, ISOPOOH, GLY, GLYALD, HYAC SOG1, SOG2A and SOG2B.

Rain-out, evaporation and wash-out are calculated after each other for large-scale and convective precipitation. Following Jacob *et al.* (2000), the fractions ($f_{i,L}$, $f_{i,I}$) of a trace gas i dissolved in cloud / rain droplets (L) or cloud ice (I) is calculated using Henry's law equilibrium:

$$\frac{C_{i,L}}{C_{i,G}} = H_i \times LRT \tag{3.34}$$

in the follwoing way:

$$f_{i,L} = \frac{C_{i,L}}{C_{i,T}} = \frac{\frac{C_{i,L}}{C_{i,G}}}{1 + \frac{C_{i,L}}{C_{i,G}} + \frac{C_{i,L}}{C_{i,G}}}$$
(3.35)

$$f_{i,I} = \frac{C_{i,I}}{C_{i,T}} = \frac{\frac{C_{i,I}}{C_{i,G}}}{1 + \frac{C_{i,L}}{C_{i,G}} + \frac{C_{i,I}}{C_{i,G}}}$$
(3.36)

 $C_{i,L}$, $C_{i,I}$, $C_{i,G}$ and $C_{i,T}$ are the concentrations of i in the droplet (L), cloud ice (I) and air (G) and the total concentration (T), repectively. H_i is the effective Henry coefficient for species i, L the (scaled) cloud liquid water content (or precipitation, in the case of below-cloud scavenging), R the ideal gas constant and T temperature. Only H_2O_2 and HNO_3 are assumed to dissolve in ice clouds (Lawrence and Crutzen, 1998), and hence subject to in-cloud ice precipitation.

The effective Henry coefficient for SO_2 and NH_3 accounts for its dissociation in water, and is calculated following (Seinfeld and Pandis, 1998), assuming a rain water acidity of pH=5.6 over oceans and pH=5 over land. The other Henry's law coefficients are taken from the compilation by (Sander, 2015).

(a) In-cloud scavenging

The loss by in-cloud scavenging (rain-out) is governed by the precipitation formation rate P_r .

The in-cloud scavenging rate $W_{i,k}^{I}$ [s⁻¹] for species i at level k is adapted from the approach of Luo *et al.* (2019). For liquid precipitation of trace gases,

$$W_{i,k}^{I} = \frac{cf \times \beta_{r,k}}{k \times q_{k,r,tot}} \exp\left(-kR_c f_{i,L} \Delta_t\right)$$
(3.37)

Rc is the retention coefficient which accounts for the retention of dissolved gas in the liquid cloud condensate as it is converted to precipitation. R = 1.0 for all species in warm clouds (T > 268 K). For mixed clouds (T < 268 K), R is 0.02 for all species but 1.0 for HNO₃ and 0.6 for H₂O₂ (von Blohn *et al.*, 2011).

A similar expression is used for in-cloud precipitation due to ice cloud, but replacing $f_{i,L}$ with $f_{i,I}$ and computing k, the rain-out loss rate, based on ice precipitation formation.

For aerosol expression 3.37 reads:

$$W_{i,k}^{I} = \frac{cf \times \beta_{r,k}}{k \times q_{k,r,tot}} \exp\left(-kD_{w,i}\Delta_{t}\right)$$
(3.38)



Table 3.9 Value of the parameter D_w , representing the the fraction of the aerosol that is embedded in the cloud liquid water.

$D_{w,i}$ value
0.9
0.7
0.7
0.7
0.7
0.8
0.9

Here $D_{w,i}$ is the fraction of aerosol that is embedded in the cloud liquid/solid water, provided by table 3.9.

In eqs 3.37 and 3.38, $\beta_{r,k}$ is the rate of new precipitation formation (rain only) and cf is the cloud fraction. $q_{k,r,tot}$ represents the condensed water content (liquid) within the grid cell and is derived from the liquid water mass mixing ratio q_k by

$$q_{k,r,tot} = q_k + \Delta_t \times \beta_{r,k} \tag{3.39}$$

where Δ_t is the time step and $\beta_{r,k}$ is defined as in Giorgi and Chameides (1986) using the rain flux $P_{r,k}$ at level k:

$$\beta_{r,k} = (P_{r,k+1} - P_{r,k}) \times (\rho_k \Delta z_k) \tag{3.40}$$

The first-order rain-out loss rate k_loss , which represents the conversion of cloud water (or ice water) to precipitation water, is then computed as:

$$k_{l}oss = \left[k_{min} + \frac{\beta_{k,r}}{q_{k,r,tot}}\right] \tag{3.41}$$

 k_{min} is the minimum value of rain-out loss rate, set to $0.0001s^{-1}$ following Luo et al. (2019).

The formulation of Luo *et al.* (2019) applies only to liquid precipitation. It has been extended for solid precipitation, but taking into account the smaller fraction of aerosols included in solid precipitation, the value the D_i parameter is divided by two for solid precipitation. The scavenging rates for solid and liquid precipitation are then added.

(b) Re-evaporation

The release of trace gases and aerosols contained in rain drops at level k occurs if evaporation of precipitation is diagnosed, i.e. if the precipitation flux at level k is higher than at level k+1, where level k+1 is below level k. If there is no precipitation at level k+1, then all aerosols that have been subjected to in-cloud scavenging at or above level k are released. If the precipitation flux at level k+1 is not null, then the re-evaporation is partial. Before cycle 46R1, it was assumed arbitrarily that half of the scavenged trace gas and aerosols at or above level k are then released. Since cycle 46R1, a more complex parameterization has been implemented, following de Bruine $et\ al.\ (2018)$. The mass of an aerosol or trace gas species i that is re-evaporated at level k is computed as a function of the fraction of evaporated precipitation defined with the precipitation flux at level k (P_k) , and the fraction of evaporated precipitation $e_k = \frac{P_{k+1} - P_k}{P_k}$:

$$\delta M_{i,k}^{evap} = \epsilon_k \times \left(\left[1 - exp^{-2\sqrt{\epsilon_k}} \left(1 + 2 \times \epsilon_k^{\frac{1}{2}} + 2 \times \epsilon_k + \frac{4}{3} \epsilon_k^{\frac{3}{2}} \right) \right] \times (1 - \epsilon_k) + \epsilon_k^2 \right) \times Loss_{scav,i,k}$$
(3.42)

Where $Loss_{scav,i,k}$ is the sum of the mass of aerosol or trace gas that is subjected to in-cloud wet deposition from level k to the model top.



Species	α_r	α_i
Seasalt fine	0.001	0.005
Seasalt coarse	0.001	0.005
Seasalt super coarse	0.1	0.005
Dust fine	0.001	0.005
Dust coarse	0.001	0.005
Dust super coarse	0.1	0.005
OM hydrophilic	0.0001	0.005
OM hydrophobic	0.0001	0.005
BC hydrophilic	0.0001	0.005
BC hydrophobic	0.0001	0.005
Sulphate	0.0001	0.005
Nitrate fine	0.0001	0.005
Nitrate coarse	0.1	0.005
Ammonium	0.0001	0.005

Table 3.10 *Value of the parameters* α_r *and* α_i .

(c) Below-cloud scavenging

The fraction W_i^B of a highly soluble tracer i that is scavenged by below-cloud scavenging (wash-out), is computed as

$$W_i^B = f\left(1 - exp\left(-k_i'\frac{P_{r,k}}{f}\Delta_t\right)\right) \tag{3.43}$$

with $P_{r,k}$ the grid-scale precipitation rate and f the precipitation area faction of the grid cell. For HNO₃, and for other trace gases for which the scavenging is limited by mass transfer $(f_{i,L} > W_i^B/f)$, equation 3.43 is adopted with a first order wash-out loss rate constant of $k'_i = 1$ cm⁻¹. If scavenging is limited by Henry solubility $(f_{i,L} < W_i^B/f)$ then the total mass of scavenged tracer transported out through the bottom of the gridbox is:

$$\Delta m_{i,bottom} = f_{i,L}(fm_i + \Delta m_{im,top}) \tag{3.44}$$

For aerosols, the below cloud scavenging rate is expressed by:

$$W_{i,k}^{B} = f p_k \times \left[\left(1 - \exp\left(P_{r,k} \times \alpha_r \right) \right) + \left(1 - \exp\left(P_{i,k} \times \alpha_i \right) \right) \right]$$
(3.45)

Where $P_{r,k}$ and $P_{i,k}$ are the fluxes of liquid and solid precipitation respectively, $f p_k$ is the fraction of grid cell at level k in which precipitation occurs, and α_r and α_i the efficiency with which aerosol variables are washed out by rain and snow, respectively. The values used have been derived from Stier *et al.* (2005) and are summarized in table 3.10.

3.2.3 Sedimentation of aerosols

Sedimentation has been left broadly unchanged since cycle 32R2 (Morcrette et~al. (2009)). In cycle 47R3 and before, It was applied only for super-coarse dust and sea-salt, for which it is an important sink. In cycle 48R1, it is applied to all aerosol tracers. The change in mass mixing ratio from sedimentation follows the approach of Tompkins (2005) for ice sedimentation. The change in mass concentration caused by a transport in flux form at velocity V_s is given by:

$$\frac{dC}{dt} = \frac{1}{\rho} \frac{d(\rho V_{\rm s}C)}{dz} \tag{3.46}$$



Table 3.11 *Sedimentation velocity for aerosol species other than sea-salt aerosol bin2 and 3*

Species	V_s (m/s)
Sea salt 1	2.4E-5
Dust 1	6.9E-5
Dust 2	1.982E-4
Dust 3	1.962E-3
OM/BC/SU/NI1/AM/SOA	2E-4
Nitrate 2	1.33E-3

where ρ is the air density. The integration of this gives for each level k and time step j:

$$C_{k+1}^{j} = \frac{\frac{\rho^{j-1} V_{s} C_{k+1}^{j-1}}{\rho^{j} \Delta Z} \Delta t + C_{k}^{j}}{1 + \frac{\rho^{j} V_{s}}{\rho^{j} \Delta Z} \Delta t}$$
(3.47)

which is solved from top to bottom. The gravitational velocity V_s is provided from an external source, the aerosol table file, and is horizontally and vertically invariant for all species except for bin2 and 3 of sea-salt aerosol, for which it is computed online using Stokes' law if the namelist entry LAERSEDIMSS is set to true (which is the case in cycle 48R1). In this case (sea-salt aerosol bin 2 and 3 and LAERSEDIMSS set to true), the settling velocity is computed as:

$$V_{\rm s} = \frac{2\rho_{\rm p}g}{9\mu} \, r^2 \, C_{\rm F} \tag{3.48}$$

where ρ_p is the particle density, g the gravitational constant, μ the air viscosity and C_F the Cunningham correction factor.

Table 3.11 provides the fixed sedimentation velocities used for the other species.

3.2.4 Code overview

The dry deposition velocities for reactive gases are calculated in DEPVEL_GC (and subroutines within), which is called in VDFMAIN before the simulation of the vertical diffusion of tracers in VDFDIFC. DEPVEL_GC requires input from the land surface scheme (Part IV Physical processes, Chapter 6), which is provided via the interface routine SURFEXCDRIVER.

AER_DRYDEP is the routine used as an interface for the calculation of the aerosol dry deposition velocities, which is called from AER_PHY2. The computation itself is carried out in AER_DRYDEPVELZH14 The update of the 3D aerosol tendencies because of sedimentation is calculated in AER_SEDIMNT, which is also called from AER_PHY2.

AER_SRC is the routine where the online emissions of desert dust are computed. AER_SRC is called from AER_PHY2. The sea-salt aerosol emissions are called from AER_SSALT_ALBERT, called from AER_SRC.



Chapter 4

Transport processes

Table of contents

- 4.1 Advection
 - 4.1.1 Overview
 - 4.1.2 Specification of SL advection and Mass fixer for tracers
- 4.2 Turbulent diffusion, injection of surface fluxes and convection

The transport of tracers by advection, vertical turbulent diffusion and convective mass fluxes is conceptually the same for aerosol and traces gases and other tracer such as humidity, cloud water and ice. This section documents the specifics for the aerosol and trace gases transport .

4.1 ADVECTION

4.1.1 Overview

The simulation of tracer advection by the three-dimensional wind fields applies the semi-Lagrangian (SL) method as outlined in Part III Dynamics and Numerical Procedures, Chapter 3, which is also used to simulate the advection of humidity and temperature. In contrast to mass-conserving flux-form advection schemes, which calculate the tracer mass flux through all grid-box boundaries, the SL scheme approximates the change of the mass mixing ratio by advection by assigning the interpolated mass mixing ratio of the departure point to the grid box value. The departure point is the point where the trajectory of an air parcel originated at the beginning of the time step. The departure point, which is the same for all advected variables, is calculated from the wind fields in an iterative way. The mass mixing ratio at the departure point is interpolated from the surrounding grid points. Different interpolation methods and limiters can be configured for each tracer field.

The SL method is computationally very efficient because the time step length is not limited by the Courant–Friedrichs–Lewy (CFL) condition. The CFL condition constrains the time step depending on the wind speed and the grid box size (resolution) for flux form advection schemes. A specific computational advantage of the SL advection scheme for atmospheric composition simulation is that the identification of the departure point, which is computationally expensive, is only required to be carried out one time independently of the number of advected tracers.

The semi-Lagrangian advection method does not formally conserve the tracer mass in contrast to flux-form based advection schemes. The local amount of mass non-conservation of the SL advection can not be correctly diagnosed and both erroneous creating and destruction of tracer mass occurs. It is only possible to calculate the global amount of tracer mass conservation by calculating the global mass of a tracer before and after the advection time step.

To enforce global mass conservation, the IFS has different options for global mass fixers (MF) (Diamantakis and Flemming, 2014). Global mass fixers (i) diagnose the global amount of mass conservation after each advection time and (ii) modify the resulting MMR to match the global tracer mass at the start of the time step. As the global mass integration depends on the surface pressure, conservation of the global surface pressure integral has to be ensured to accurately diagnose the mass non-conservation.

The local corrections of any MF approach are always positive or always negative depending on the sign of the global mass non-conservation. The global mass fixers implemented in the IFS uses different



methods to locally modify the MMR. The proportional MF in the IFS scales all grid point MMR values with the same correction factor. There are also MF that apply locally varying amount of mass depending on conditions such as the smoothness of the tracer field or the approximated accuracy of the interpolation of the departure point value (Part III Dynamics and Numerical Procedures, Section 3.2.5).

4.1.2 Specification of SL advection and Mass fixer for tracers

The specification of the options for SL-advection and MF are specified in a name-list (NAMGFL). Only one type of global MF can be selected for all tracers, which can be specifically configured for each tracer. The configuration for CY48R1 is summarised in table 4.1 and explained below.

All Greenhouse gases, aerosols and most reactive gas species are advected. Only very short-lived chemical species such as OH, HO2 and H radical are not advected because the chemical lifetime is smaller than the advection time step. The MMR tendencies of these very-short-lived species are entirely controlled by the chemical conversion.

Item	GHG	Aerosols	Chemistry
Advected species	all	all	excluding very-short-lived
Family advection	none	none	NO_y , Br_y , Cl_y
Quasi Monotonic limiter	3D	3D	3D
COMAD interpolation	horizontal	horizontal	horizontal
Mass fixer	3D Bermejo-Conde	proportional	proportional

Table 4.1 configuration of SL interpolation and global mass fixers in CY48R1.

(a) Departure point interpolation

The COntinuous Mapping About Departure points (Malardel and Ricard, 2015, COMAD) scheme is used for the interpolation to the departure point. The COMAD scheme improves the mass conserving property of the SL advection scheme by modifying the interpolation weights. This is achieved by using the size of the grid cell at the arrival point for computations at the departure point. The COMAD scheme is only applied for the horizontal interpolation.

For the vertical interpolation quasi-monotonic cubic interpolation method is used.

Further, a quasi-monotone limiter of the interpolated departure point value is applied prevent overshoots/undershoots by limiting the interpolated values to the range of surrounding grid points in horizontal and vertical direction (LQM3D).

(b) Family advection

Groups of chemical species (families) such as oxidised nitrogen components are characterised by quick chemical conversions leading to large spatial gradients for example near the day-night terminator. As the SL advection has the tendency to suffer from larger mass conservation errors in areas of large gradient, the individual advection of each family member can lead to drift and issues of nonconservation. Therefore the chemical species of the family are added to a single family tracer, which is advected and subject to MF application. The individual MMR for each family member is calculated after the advection from the proportional contribution to the family at the start of the time step. The family advection approach is applied to the following chemical families:

- Bromine family (BrCl, HOBr, BrONO₂, Br, HBr, BrO and Br₂)
- Chlorine family (Cl₂O₂, OClO, BrCl, HOCl, ClONO₂, Cl, HCl, ClO, ClNO₂, Cl₂ and ClOO)
- NOy family (N, NO, NO₂, NO₃, HO₂NO₂, N₂O₅, HNO₃, ClNO₂, ClONO₂ and BrONO₂)

(c) Global mass fixing

The IFS tracer MF extends the method of Bermejo and Conde (2002) (BC, LTRCMFBC=true) as described in Agusti-Panareda *et al.* (2017) and Diamantakis and Agusti-Panareda (2017) for Greenhouse Gases.



For the aerosol and reactive gases the proportional MF is applied. The BC MF computes a correction to the transported field with its magnitude depending on the local smoothness of the field with larger corrections in locations of large gradients. A detailed description of the BC MF scheme is provided in Part III Dynamics and Numerical Procedures, Section 3.2.5.

The BC MF type is the multiplicative standard configuration (NOPTMFBC=3). The species specific-smoothness parameter (BETAMFBC=2) is set for GHG in such a way that the MF applies smaller corrections in areas, where the tracer gradient is close to zero. As only one mass fixer type can be selected in the IFS, setting BETAMFC=-999 for all advected aerosol and chemistry species makes the BC configuration act as the proportional MF, which applies the mass conservation correction by a globally constant scaling factor.

The choices for SL scheme interpolation and the MF have been determined empirically for GHGs, aerosol and reactive gases and will be further reviewed. The more conservative choice for the proportional MF for aerosol and reactive gases, is motivated by the lack of stronger localised changes of the MMR compared to the BC MF. The main motivation for the choice of the BC MF for GHG is its tendency to modified less the very smooth background field throughout the atmosphere.

4.2 TURBULENT DIFFUSION, INJECTION OF SURFACE FLUXES AND CONVECTION

The vertical transport of tracer by diffusion follows the treatment of heat and moisture and is explained in more detail in Part IV Physical processes, Section 3.7.

The flux boundary conditions at surface are the added fluxes of emissions 3.1 from inventories and online simulation and from the dry deposition flux $-\rho V_d C$. It should be noted that the direct coupling of the surface emissions to the tracer diffusion scheme differes from the injection of emissions from elevated sources (see (d)). The elevated emissions lead to a positive mass mixing ration tendency in the model layers and the process of tubulent diffusion is applied on the updated MMR profile.

The tracer transport by cumulus convection is outlined in Part IV Physical processes, Section 6.2 based on the parameterised updraught and downdraught mass fluxes.

The routine for the tracer vertical diffusions is VDFDIFC called from VDFMAIN. The routine for the tracer convective transport is CUTRACER called from CUMASTRN.



Chapter 5

Diagnostic variables and radiative impact of aerosol

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- 5.1 Aerosol optical diagnostics
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 - 5.1.5 Other vertically integrated diagnostics in the IFS: single scattering albedo and asymmetry parameter
 - 5.1.6 3D diagnostics: extinction coefficient, SSA and backscatter
- 5.2 Particulate matter diagnostics (PM2.5, PM10)
- 5.3 Global Mass diagnostics

Appendix A. Refractive indizies

Aerosol optical depth (AOD) observations from the AERONET network (Holben *et al.*, 1998) or from VIIRS, MODIS, Sentinel 3 and other remote sensing instruments are the most common observation type to evaluate aerosol products, and AOD values retrieved from satellite observations are used for the aerosol data assimilation. Hence, the correctness of the calculation of the radiative impact of aerosol on atmospheric radiation is important for the evaluation and the successful assimilation of AOD satellite retrievals

Further frequently observed in-situ parameter are particulate matter concentration below a diameter of 10 or $2.5 \mu m$

5.1 AEROSOL OPTICAL DIAGNOSTICS

5.1.1 introduction

The aerosol optical diagnostics are computed in the routine AER_BDGTMSS, called from AER_PHY3. As shown in Figure 5.1, the aerosol optical diagnostics are computed using aerosol optical properties, which are computed offline with a Mie code for each aerosol species and bin, and for a selection of wavelengths. These aerosol optical properties are saved into a netcdf file, which is read as part of the radiation scheme. These aerosol optical properties are then stored into IFS arrays, which are used together with the simulated mass mixing ratio of each aerosol tracer and air density to compute the extinction by each aerosol species: it thus depends on its abundance (mass mixing ratio) and its mass extinction, which is dependent on the wavelength and differs significantly from one species to the other. In this section, we describe the inputs of the offline Mie code, and how they are used online to compute aerosol optical diagnostics.

5.1.2 Offline computations of aerosol optical properties

The Mie theory (Wiscombe, 1980) is a mathematical-physical theory of scattering of scattering of electromagnetic waves by homogeneous spherical particles. It is an adequate method to estimate the scattering, the absorbing and the extinction efficiency of spherical homogeneous particles, for particles that have a size in the same order of magnitude as the wavelength considered. From these efficiencies the following four bulk optical aerosol properties are derived which are used in the IFS to compute aerosol



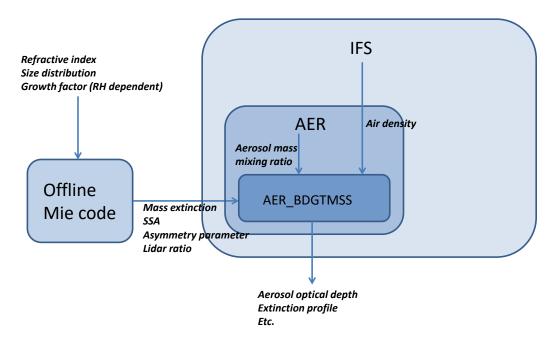


Figure 5.1 Schematic showing how the aerosol optical diagnostics are computed, using aerosol optical properties that are computed offline with a Mie code, loaded and stored as arrays in the IFS, and used together with the mass mixing ratio of each aerosol species, and air density.

optical diagnostics: (i) mass extinction, (ii) single scattering albedo (SSA), (iii) asymmetry parameter and (iv) lidar ratio. The Mie theory uses the complex refractive indezies as input, which depend on the chemical composition of the particles and information about the assumed size distribution of the particles and their density.

The sofware (fortran) that does the Mie theory calculation is used offline to compute the bulk aerosol optical properties for each species for each of the 14 short-wave (SW) and 16 long-wave (LW) bands of the RRTM radiation scheme on which the IFS radiation scheme is based (ecRad, (Hogan and Bozzo, 2018)) as well as for each of 20 wavelengths used for IFS-AER output. Spherical shape is assumed for all species. The number size distribution n(r) is described by a log-normal function in general similar to the original version of the aerosol scheme (Reddy *et al.*, 2005):

$$n(r) = \frac{dN(r)}{dr} = \frac{N}{\sqrt{2\pi}r\ln(\sigma)} exp\left(-\frac{\ln^2(r/r_{mod})}{2\ln^2(\sigma)}\right)$$
 (5.1)

with N total particle number concentration, σ geometric standard deviation and r_{mod} mode radius.

Table 5.1 lists the relevant parameters of the assumed number size distribution for each species. It should be noted that this assumed size distribution is used for the offline computation of aerosol optical properties with the Mie code only. For dust, the number size distribution specific are from (Ryder *et al.*, 2018). The bulk optical properties (mass extinction coefficient, single scattering albedo (ω) and asymmetry parameter (g)) are computed with a standard code for Mie scattering based on (Wiscombe, 1980). The size bin limits and density of the aerosol species is given in 2.2. For the hydrophilic types the optical properties change with the relative humidity due to the swelling of the water soluble component in wetter environments. The refractive index (m) and density (ρ) of the aerosol particle change according to the relations:



Table 5.1 Aerosol species and parameters of the number size distribution associated to each aerosol type of AER as used in the off-line Mie calcualtions. (r_{mod} =mode radius, ρ =particle density, σ =geometric standard deviation), Number (where relevant). **Values are for the dry aerosol apart from sea salt which is given at 80% RH.**. The number size distribution is assumed to be monomodal for all species except for dust (four modes used in cycle 48R1, but monomodal up to cycle 47R3 include), sea salt aerosols and coarse mode nitrate for which a bimodal size distribution is assumed.

Aerosol type	r _{mod} (µm)	σ	Number cm ⁻³
Sea Salt (80% RH)	0.1992,1.992	1.9,2.0	70,3
Dust	0.05,0.42,0.79,16.2	2.2,1.18,1.93,1.53	391,8.39,11.6,0.000138
Black carbon	0.0118	2.0	
Organic matter	0.09	1.6	
Sulfates	0.0355	2.0	
Nitrate fine	0.0355	2.0	
Nitrate coarse	0.199,1.992	1.9,2.0	70,3
Ammonium	0.0355	2.0	
SOA	0.09	1.6	

$$\rho = \rho_{dry} * r_{dry}^3 / r^3 + \rho_{water} * (r^3 - r_{dry}^3) / r^3$$
(5.2a)

$$m = m_{water} + (m_{dry} - m_{water}) * r_{dry}^3 / r^3$$
 (5.2b)

with r_{dry} and r the mode radius respectively of the dry particle and at a relative humidity value. The size distribution is modified applying growth factors to the mode radius and to the limits of integration, maintaining the same geometric standard deviation.

Information about the size distribution, particle density and refractive index is used in the Mie code to compute mass extinction, single scattering albedo (SSA) and asymmetry parameter. Figure 5.2 gives an example of mass extinction and absorption coefficients for desert dust, as used in cycle 48R1.

5.1.3 Refractive index and growth factors for off-line Mie calculations

(a) Sea-salt aerosol

The sea-salt refractive index are from the Optical Properties of Aerosols and Clouds (OPAC) database (Hess *et al.*, 1998). They are shown in Table A.1.

The assumed hygroscopic growth is shown in Table 5.2

(b) Desert dust

The refractive index for dust for the 200-1000nm spectral range have been derived from a simulation using an experimental version of IFS-COMPO that represents twelve dust mineralogical species. For the 1000 to 3000nm range, we used values provided by (Balkanski *et al.*, 2007), who propose different values with different assumptions for the relative abundance of hematite (0.9, 1.5 and 2.7% hematite fraction of total volume). The refractive index chosen was with 0.9% hematite , which is their low value for hematite but which is much higher than the simulated fraction of dust that consists of hematite as provided by the climatology of dust mineralogy (0.22% average for 2017-2020). Finally, for the 3000-10000nm, the refractive indexes proposed by (Di Biagio *et al.*, 2017) have been used. Regional values are proposed that reflect the changing composition of dust; the values for the Bodele depression have been chosen. The refractive index of dust is shown in table A.3.



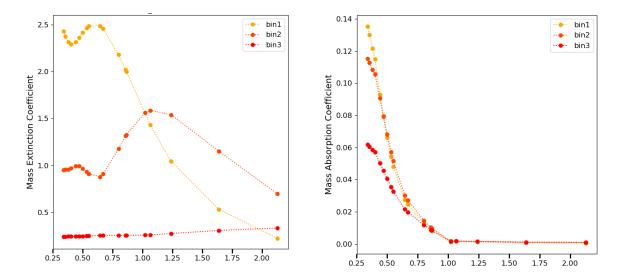


Figure 5.2 Desert dust: mass extinction (left) and absorption (right) coefficients as a function of wavelength in μ m. Values are shown for the three bins, from fine to super-coarse. The mass absorption coefficient is computed as mass extinction x (1 - SSA). Values are shown for three dust bins.

(c) Organic matter

In cycle 48R1, with the introduction of a specific Secondary Organic Aerosol species, OM includes only primary OM, while in previous cycles, OM included both primary and secondary organics. The optical properties from (Brown *et al.*, 2018) have been implemented for the OM species in cycle 48R1. Figure 5.3 shows how mass extinction and single scattering albedo are impacted by the new set of optical properties. Extinction is significantly higher with the new optical properties, especially for low relative humidities. The SSA, which determines how absorbing is OM, differs also significantly. The current set of optical properties give SSA that are continuously decreasing with increasing wavelength. The (Brown *et al.*, 2018) refractive index give a SSA that is lower and thus more absorbing OM for smaller wavelengths, in the UV and near-UV, which is a signature of brown carbon. This in turn translates into much higher mass absorption coefficient (MAC) for UV and to a lesser extent visible wavelengths. MAC in the IR is on the other hand lower with the (Brown *et al.*, 2018) refractive index as compared to the OM optics used in cycle 47R3 and before.

Tables A.4 and 5.2 show the refractive index and hygroscopic growth factors used for organic matter. The hydrophobic tracer uses values at 20% relative humidity.

(d) Black carbon

The black carbon refractive index are from the Optical Properties of Aerosols and Clouds (OPAC) database (Hess *et al.*, 1998), with a value at 500nm of 1.75 for the real part and 0.45i for the imaginary part.

(e) Sulfate

A scaling factor on mass extinction of 1.375 is used up to CY47R3, which meant to represent the ratio in molar masses between ammonium sulfate and sulfate. In CY48R1, it is used only if ammonium is not included in the aerosol tracers. The refractive index is taken from the Global Aerosol Climatology Project (GACP, http://gacp.giss.nasa.gov/data_sets/) and it is representative of dry ammonium sulfate. The growth factors shown in Table 5.2 are from (Tang and Munkelwitz, 1994)



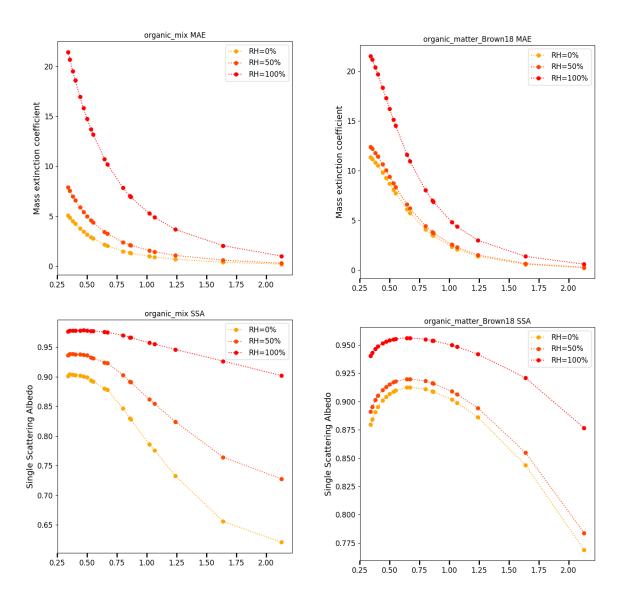


Figure 5.3 Organic matter: mass extinction coefficient or efficience in m^2/g (top) and single scattering albedo (bottom) as a function of wavelength in μm for cycle 47R3 and before (left) and 48R1 (right). Values are shown for 0, 50 and 100 % relative humidity.

(f) Nitrate

The refractive index for nitrate from gas/particle partitioning ("nitrate 1" or "fine mode nitrate") use a spectrally constant value of 1.611 for the real part, and 0i for the imaginary part. The refractive index of nitrate from heterogeneous reactions ("nitrate 2" or "coarse mode nitrate") uses a spectrally constant value of 1.51 for the real part and 0.001i for the imaginary part of the complex refractive index. Its values are shown in Table A.5. The hygroscopic growth is shown in Table 5.2.

(g) Ammonium

Ammonium uses similar refractive index as for sulfate. No scaling factor is applied for extinction. Similarly, the growth factor used is the same as that of sulfate.



Table 5.2 Hygroscopic growth of AER aerosol

RH	0	10	20	30	40	50	60	70	80	85	90	95
Sea Salt	0.503	0.503	0.503	0.503	0.724	0.782	0.838	0.905	1	1.072	1.188	1.447
Organic matter	1	1	1	1	1	1.05	1.1	1.15	1.2	1.25	1.3	1.4
Sulfate	1	1	1	1	1.169	1.22	1.282	1.363	1.485	1.581	1.732	2.085
Nitrates	1	1.1	1.2	1.3	1.35	1.4	1.5	1.6	1.7	1.8	2.	2.2
SOA	1	1	1	1	1	1.2	1.3	1.4	1.5	1.6	1.7	1.8

(h) Secondary organic aerosol

Following (Moise *et al.*, 2015), the anthropogenic and biogenic SOA tracers use slightly different real parts of the refractive index: a spectrally constant value of 1.5 for anthropogenic SOA and 1.4 for biogenic SOA. For the two tracers, a spectrally constant value of 0.01i is used for the imaginary part. The hygroscopic growth of SOA is shown in table 5.2

5.1.4 Aerosol optical depth calculation

AOD is computed online in the IFS in the AER_BDGTMSS routine. The mass extinction for each species (computed offline and stored as look-up tables in arrays) is multiplied to air density as well as the mass mixing ratio to obtain model level extinction for each aerosol species, which is then summed over all aerosol species to obtain total aerosol extinction at each model level. Vertical integration is then carried out to compute total AOD at each of the 20 following wavelengths: 340, 355, 380, 400, 440, 469, 500, 532, 555, 645, 670, 800, 858, 865, 1020, 1064, 1240, 1640, 2130 and 10000 nm.

The aerosol absorption is computed for each species and each model level by multiplying the simulated aerosol extinction by (1 - SSA) where SSA is the single scattering albedo computed offline by the Mie code. Similarly to AOD, this is then summed over species and integrated over the vertical to provide absorption AOD (AAOD) at each of the 20 wavelengths.

5.1.5 Other vertically integrated diagnostics in the IFS: single scattering albedo and asymmetry parameter

In addition to AOD, vertically integrated SSA and asymmetry parameter are also provided. They are computed as the sum of the values for each aerosol species. For each aerosol species, the vertically integrated SSA and asymmetry parameter is computed as the integral over the vertical of the species's SSA and asymmetry parameter (which is independent of height) weighted by the model level extinction coefficient for the concerned aerosol species. The vertically integrated SSA and asymmetry parameter are proposed for the 20 wavelengths mentioned above.

5.1.6 3D diagnostics: extinction coefficient, SSA and backscatter

If the namelist swith LAERLISI is set to true, a selection of 3D diagnostic of aerosol optical properties are also available over all of the model levels, only at the 355, 532 and 1064 nm wavelengths. These consists of:

- Extinction coefficient (sum of all species),
- Single Scattering Albedo, defined as 1 AAOD/Extinction coefficient,
- Aerosol backscatter from top of atmosphere,
- Aerosol backscatter from surface,
- Unattenuated molecular backscatter coefficient,
- Unattenuated aerosol backscatter coefficient,

The 3D Extinction coefficient and SSA are computed in AER_BDGTMSS. The other 3D diagnostics are called in the routine AER_LIDSIM, called from AER_BDGTMSS if the LAERLISI namelist switch is true. The last four fields are computed using the lidar ratio, itself computed offline for each aerosol species by the Mie code.



5.2 PARTICULATE MATTER DIAGNOSTICS (PM2.5, PM10)

Particulate Matter smaller than 1, 2.5 and 10 μm are important outputs of IFS-COMPO. They are computed with the following formulae that uses the mass mixing ratio from each aerosol tracer as an input, denoted $[SS_{1,2,3}]$ for seasalt aerosol, $[DD_{1,2,3}]$ for desert dust, $[NI_{1,2}]$ for nitrate, [OM], [BC], [SU], [NI], [AM], [SOA] for Organic Matter, Black Carbon, Sulfate, Nitrate, Ammonium and SOA respectively:

$$\begin{split} PM_1 &= \rho \Big(\frac{[SS_1]}{4.3} + 0.97[DD_1] + 0.6[OM] + [BC] + 0.6[SU] + 0.6[NI_1] + 0.6[AM] + 0.6[SOA] \Big) \\ PM_{2.5} &= \rho \Big(\frac{[SS_1]}{4.3} + 0.5 \frac{[SS_2]}{4.3} + [DD_1] + [DD_2] + 0.7([OM] + [BC] + [SU] + [NI_1] + [AM] + [SOA]) + 0.25[NI_2] \Big) \\ PM_{10} &= \rho \Big(\frac{[SS_1]}{4.3} + \frac{[SS_2]}{4.3} + [DD_1] + [DD_2] + 0.4[DD_3] + [OM] + [BC] + [SU] + [NI_1] + [NI_2] + [AM] + [SOA] \Big) \end{split}$$

where ρ is the air density. The sea-salt aerosol tracers are divided by 4.3 so as to transform the mass mixing ratio at 80% ambiant relative humidity to dry mass mixing ratio.

5.3 GLOBAL MASS DIAGNOSTICS

Besides diagnostic output as fields at the model resolution, the IFS can calculate global diagnostic of the (i) atmospheric and (ii) tropospheric burden and the global values of sink and source terms such as (iii) emissions, (iv) dry deposition, (v) wet deposition and (iv) chemical conversion. These values are stored in text files and are useful to compare global sink and source terms in a convenient way, without the need to retrieve grid-point fields. The global mass diagnostics work for all tracers and are switched on with LCHEM_DIA=true.



APPENDIX A. REFRACTIVE INDIZIES

Table A.1 *Refractive index for sea-salt aerosol at* 0% *relative humidity, as a function of wavelength*

Wavelength (m)	Real part	Imaginary part
0.250E-06	1.510000	5.000000e-06
0.300E-06	1.510000	2.000000e-06
0.350E-06	1.510000	3.240000e-07
0.400E-06	1.500000	3.000000e-08
0.450E-06	1.500000	2.430000e-08
0.500E-06	1.500000	1.550000e-08
0.550E-06	1.500000	1.000000e-08
0.600E-06	1.490000	1.600000e-08
0.650E-06	1.490000	4.240000e-08
0.700E-06	1.490000	2.000000e-07
0.750E-06	1.490000	1.080000e-06
0.800E-06	1.480000	1.950000e-06
0.900E-06	1.480000	4.240000e-05
1.000E-06	1.470000	1.410000e-04
1.250E-06	1.470000	3.580000e-04
1.500E-06	1.460000	5.700000e-04
1.750E-06	1.450000	7.620000e-04
2.000E-06	1.450000	1.000000e-03
2.500E-06	1.430000	4.000000e-03
3.000E-06	1.610000	1.000000e-02
3.200E-06	1.490000	3.000000e-03
3.390E-06	1.480000	2.050000e-03
3.500E-06	1.480000	1.600000e-03
3.750E-06	1.470000	1.400000e-03
4.000E-06	1.480000	1.400000e-03
4.500E-06	1.490000	1.400000e-03
5.000E-06	1.470000	2.500000e-03
5.500E-06	1.420000	3.600000e-03
6.000E-06	1.410000	1.100000e-02
6.200E-06	1.600000	2.200000e-02
6.500E-06	1.460000	5.000000e-03
7.200E-06	1.420000	7.000000e-03
7.900E-06	1.400000	1.300000e-02
8.200E-06	1.420000	2.000000e-02
8.500E-06	1.480000	2.600000e-02
8.700E-06	1.600000	3.000000e-02
9.000E-06	1.650000	2.800000e-02
9.200E-06	1.610000	2.620000e-02
9.500E-06	1.580000	1.800000e-02
9.800E-06	1.560000	1.600000e-02
10.000E-06	1.540000	1.500000e-02



Table A.2 *Refractive index for sea-salt aerosol at* 0% *relative humidity, as a function of wavelength*

Wavelength (m)	Real part	Imaginary part
10.600E-06	1.500000	1.400000e-02
11.000E-06	1.480000	1.400000e-02
11.500E-06	1.480000	1.400000e-02
12.500E-06	1.420000	1.600000e-02
13.000E-06	1.410000	1.800000e-02
14.000E-06	1.410000	2.300000e-02
14.800E-06	1.430000	3.000000e-02
15.000E-06	1.450000	3.500000e-02
16.400E-06	1.560000	9.000000e-02
17.200E-06	1.740000	1.200000e-01
18.000E-06	1.780000	1.300000e-01
18.500E-06	1.770000	1.350000e-01
20.000E-06	1.760000	1.520000e-01
21.300E-06	1.760000	1.650000e-01
22.500E-06	1.760000	1.800000e-01
25.000E-06	1.760000	2.050000e-01
27.900E-06	1.770000	2.750000e-01
30.000E-06	1.770000	3.000000e-01
35.000E-06	1.760000	5.000000e-01
40.000E-06	1.740000	1.000000e+00



 Table A.3 Refractive index for desert dust, as a function of wavelength

Wavelength (m)	Real part	Imaginary part
0.2000E-06	0.1530E+01	0.8000E-01
0.3000E-06	0.1530E+01	0.1800E-01
0.4000E-06	0.1530E+01	0.9000E-02
0.5000E-06	0.1530E+01	0.5700E-02
0.6000E-06	0.1530E+01	0.4700E-02
0.7000E-06	0.1530E+01	0.3600E-02
0.8000E-06	0.1520E+01	0.4300E-02
0.9000E-06	0.1520E+01	0.4300E-02
0.1000E-05	0.1520E+01	0.4500E-02
0.1536E-05	0.1400E+01	0.4500E-02
0.2000E-05	0.1260E+01	0.4500E-02
0.2250E-05	0.1220E+01	0.4500E-02
0.3000E-05	0.1160E+01	0.3500E-01
0.4000E-05	0.1260E+01	0.2100E-01
0.5000E-05	0.1250E+01	0.1500E-01
0.6000E-05	0.1150E+01	0.6000E-01
0.6500E-05	0.1130E+01	0.1000E+00
0.7200E-05	0.1400E+01	0.1700E+00
0.8000E-05	0.1150E+01	0.7800E-01
0.8200E-05	0.1130E+01	0.1100E+00
0.9000E-05	0.1700E+01	0.2650E+00
0.1000E-04	0.1750E+01	0.5360E+00
0.1150E-04	0.1590E+01	0.1200E+00
0.1200E-04	0.1550E+01	0.1240E+00
0.1300E-04	0.1470E+01	0.2380E+00
0.1720E-04	0.1630E+01	0.1920E+00
0.2000E-04	0.1680E+01	0.5360E+00
0.2500E-04	0.1970E+01	0.6000E+00
0.3000E-04	0.1800E+01	0.6300E+00
0.3500E-04	0.1900E+01	0.6300E+00
0.4000E-04	0.2100E+01	0.6300E+00



 Table A.4 Refractive index for organic matter, as a function of wavelength

Wavelength (m)	Real part	Imaginary part
0.200E-06	1.7105	0.0294772786667372
0.400E-06	1.7045	0.0244591212418513
0.600E-06	1.6985	0.0219296481995005
0.800E-06	1.6925	0.0202952456597922
1.000E-06	1.6865	0.0191118687903374
1.200E-06	1.6805	0.0181963854318748
1.400E-06	1.6745	0.0174566535040615
1.600E-06	1.6685	0.0168402205589679
1.800E-06	1.6625	0.0163145816678297
2.000E-06	1.6565	0.0158582995800324
2.200E-06	1.6505	0.0154565453837116
2.400E-06	1.6445	0.0150986664160388
2.600E-06	1.6385	0.0147767716294706
2.800E-06	1.6325	0.0144848650840567
3.000E-06	1.6265	0.0142182921207056
3.200E-06	1.6205	0.0139733725439216
3.400E-06	1.6145	0.0137471501921122
3.600E-06	1.6085	0.0135372174458498
3.800E-06	1.6025	0.0133415894234761
4.000E-06	1.5965	0.0131586119771397
4.200E-06	1.5905	0.0129868932072291
4.400E-06	1.5845	0.0128252516724681
4.600E-06	1.5785	0.0126726766666984
4.800E-06	1.5725	0.0125282973586326
5.000E-06	1.5665	0.0123913585371517
5.200E-06	1.5605	0.0122612013454353
5.400E-06	1.5545	0.012137247828825
5.490E-06	1.5518	0.0120833546953075
5.990E-06	1.5368	0.0118030958451163
6.490E-06	1.5218	0.0115510613542545
6.990E-06	1.5068	0.0113225413536594
7.490E-06	1.4918	0.0111138810095052
7.990E-06	1.4768	0.0109221916183854
8.490E-06	1.4618	0.0107451534799538
8.990E-06	1.4468	0.0105808778246553
9.490E-06	1.4318	0.0104278078762683
9.990E-06	1.4168	0.0102846465235916
10.490E-06	1.4018	0.0101503024989424
11.990E-06 13.490E-06	1.3568	0.00979155880834447
	1.3118	0.0094856952696089
14.990E-06 16.490E-06	1.2668 1.2218	0.00922021773661187 0.00898648599305493
17.990E-06	1.2218	0.00898648599305493
17.990E-06 19.490E-06	1.1768	0.00877829453865847
20.990E-06	1.1318	0.00842125327771081
20.990E-06 22.490E-06	1.0868	0.00826620162355337
23.990E-06	0.9968	0.00812374999946372
23.77UE-U0	0.7700	0.000123/47777403/2



Table A.5 Refractive index for sulfate at 0% RH, as a function of wavelength

Wavelength (m)	Real part	Imaginary part
0.200E-06	1.565000	1.000000e-07
0.400E-06	1.540300	1.000000e-07
0.600E-06	1.527300	1.000000e-07
0.800E-06	1.519700	1.000000e-07
1.000E-06	1.512300	3.500260e-07
1.200E-06	1.504800	3.400170e-06
1.400E-06	1.497300	1.100020e-05
1.600E-06	1.489800	1.900200e-04
1.800E-06	1.482000	7.599760e-05
2.000E-06	1.473000	1.000000e-03
2.200E-06	1.463000	1.699810e-03
2.400E-06	1.449900	4.499870e-04
2.600E-06	1.428000	6.807700e-04
2.800E-06	1.391600	6.552390e-03
3.000E-06	1.289700	1.024240e-01
3.200E-06	1.490700	2.508420e-01
3.400E-06	1.607100	1.639830e-01
3.600E-06	1.627000	8.410070e-02
3.800E-06	1.570000	2.734010e-02
4.000E-06	1.543000	1.528970e-02
4.200E-06	1.523000	1.142350e-02
4.400E-06	1.505400	8.402340e-03
4.600E-06	1.490000	6.686520e-03
4.800E-06	1.476600	5.934720e-03
5.000E-06	1.462900	6.148940e-03
5.200E-06	1.445700	6.807330e-03
5.400E-06	1.426582	7.490120e-03
5.490E-06	1.418048	7.810950e-03
5.990E-06	1.353414	1.174680e-02
6.490E-06	1.224115	4.102270e-02
6.990E-06	1.004190	7.888260e-01
7.490E-06	1.610615	1.047550e-01
7.990E-06	1.315695	7.914190e-02
8.490E-06	0.859320	2.750770e-01
8.990E-06	0.923574	1.626800e+00
9.490E-06	2.725528	6.138340e-01
9.990E-06	2.197668	1.329510e-01
10.490E-06	1.993193	6.076220e-02
11.990E-06	1.792637	2.020310e-02
13.490E-06	1.688341	2.003190e-02
14.990E-06	1.543961	2.223400e-02
16.490E-06	2.757855	2.956680e-01
17.990E-06	1.783815	2.191460e-02
19.490E-06	1.708317	1.877450e-02
20.990E-06	1.65598	2.357060e-02
22.490E-06	1.612242	3.164590e-02
23.990E-06	1.577303	4.125900e-02



Chapter 6

Data assimilation of atmospheric composition retrievals

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6.1 DATA ASSIMILATION METHOD

6.1.1 4DVAR method

The IFS uses an incremental four-dimensional variational (4D-Var) data assimilation system going back to Courtier *et al.* (1994). It is described in detail in Part II Data assimilation of the IFS documentation and we only repeat the basics here before describing composition-specific aspects, with particular focus on the background errors and the observation operators used for the atmospheric composition control variables. Several atmospheric composition fields, namely O3, NO2, CO, SO2, Volcanic SO2, HCHO, CO2, CH4 and aerosol total mixing ratio are included in the control vector and minimised together with the meteorological control variables. The IFS-COMPO o-suite uses 12-hour assimilation windows from 03 UTC to 15 UTC and 15 UTC to 03 UTC, and two minimisations at spectral truncations T95 (\sim 210 km) and T159 (\sim 110 km). The IFS-GHG o-suite uses the same assimilation window used in the NWP setup (09 UTC to 21 UTC and 21 UTC to 09 UTC) and performs three minimisations at spectral truncations T159 (\sim 110 km), T191 (\sim 100 km) and T255 (\sim 78 km). The assimilation window of the IFS-COMPO setup differs from the ECMWF NWP setup to allow it to run timely enough to provide boundary conditions for the CAMS regional ensemble. The IFS-GHG o-suite (assimilating CH4 and CO2 retrievals) runs independently from the IFS-COMPO o-suite.

In the current atmospheric composition 4D-Var setup, a cost function that measures the differences between the model fields and the corresponding observations is minimised to obtain the best possible forecast through the length of the assimilation window by adjusting the initial conditions. In its incremental formulation (Courtier *et al.*, 1994) this cost function can be written as:

$$J(\delta \mathbf{x}) = \frac{1}{2} \delta \mathbf{x}^{\mathrm{T}} \mathbf{B}^{-1} \delta \mathbf{x} + \frac{1}{2} (\mathbf{H} \delta \mathbf{x} - \mathbf{d})^{\mathrm{T}} \mathbf{R}^{-1} (\mathbf{H} \delta \mathbf{x} - \mathbf{d})$$
(6.1)

Here δx is the increment and at the minimum the resulting analysis increment δx^a is added to the background x^b in order to provide the analysis x^a given by

$$\mathbf{x}^{\mathbf{a}} = \mathbf{x}^{\mathbf{b}} + \delta \mathbf{x}^{\mathbf{a}} \tag{6.2}$$



 \mathbf{B} is the covariance matrix of background error while \mathbf{d} is the innovation vector

$$\mathbf{d} = \mathbf{v}^{0} - H\mathbf{x}^{b} \tag{6.3}$$

where \mathbf{y}^{o} is the observation vector. \mathbf{H} is a suitable low-resolution linear approximation of the observation operator H in the vicinity of \mathbf{x}^{b} , and \mathbf{R} is the covariance matrix of observation errors. The incremental formulation of 3D/4D-Var consists therefore of solving for $\delta \mathbf{x}$ the inverse problem defined by the (direct) observation operator \mathbf{H} , given the innovation vector \mathbf{d} and the background constraint.

6.1.2 COMPO/GHG control variables

The majority of the COMPO and GHG variables in the control vector are straightforward representations of the fields in question, e.g. O3, CO, CO2, CH4 and HCHO. However, aerosols, NO2, SO2 and Volcanic SO2 (VSO2) are more complex. The aerosol model used in the IFS-COMPO configuration of the IFS consists of 16 bins (Chapter 2.2) and yet only total AOD observations are used in the system. Total AOD does not contain sufficient information to constrain each of the individual bins and so instead a total aerosol mass mixing ratio, defined as the sum of the aerosol species, is used as the control variable in the assimilation process.

For NO2, a logarithmic control variable is used because if the analysis were based on a linear mixing ratio scale it would be prone to large extrapolation errors due to the high variability of NO2 in space and time.

SO2 and Volcanic SO2 both currently refer only to the SO2 coming from volcanic eruptions and NOT anthropogenic SO2. The difference between the two fields is that the SO2 is part of the full coupled chemistry-aerosol system and the observations are total column SO2 observations with a flag identifying them as volcanic. In contrast the Volcanic SO2 tracer simply has a prescribed lifetime of 7 days and is used with volcanic SO2 observations that contain information about the altitude of the volcanic plume.

6.1.3 Background error representation and estimation

In the IFS 4D-var data assimilation system, the background error covariance matrix is represented in operator form (Bonavita *et al.*, 2012), decomposing it into standard deviations and correlations,

$$\mathbf{B} = \mathbf{T}^{-1} \mathbf{\Sigma}_{h}^{1/2} \mathbf{C} \mathbf{\Sigma}_{h}^{1/2} \mathbf{T}^{-T}$$
 (6.4)

where T is a matrix representation of the balance operator, $\Sigma_b^{1/2}$ is the diagonal matrix of background error standard deviations and C is the background error correlation operator. The correlations, C, are given in a wavelet formulation (Fisher, 2004, 2006), which allows for both spatial and spectral variations of the background error covariances. The wavelet formulation is covered in detail in Part II Data assimilation, Section S4.2.1. The total background error covariance matrix is assumed to be block diagonal, so there are no correlations between variables. In the IFS-COMPO configuration, the correlations defined in the wavelet are climatological and hence are static in time for both the COMPO and the NWP fields. The NWP part of the correlation operator is purely the climatological information used in the NWP configuration, which is combined with the EDA errors of the day when run operational for NWP (Bonavita *et al.*, 2016). Conversely, the correlations used for the NWP fields in the IFS-GHG setup are derived from the hybrid wavelet file produced operationally for the same cycle, in which climatological information is combined with the errors of the day coming from the EDA. The formulation of the part of the correlation operator related to both the GHG and the COMPO fields is discussed in more detail below.

The background error standard deviations, $\Sigma_b^{1/2}$, are currently climatological time-constant values for both COMPO and GHG fields. They vary vertically through the atmosphere but are a globally constant value at each model level. In the IFS-COMPO configuration, the NWP standard deviations also have fixed climatological values, although a different set of standard deviations is used in each of the four seasons. In the GHG setup, the NWP standard deviations are instead derived from the errors of the day produced by the operational EDA. Furthermore, in contrast to the COMPO and the GHG fields, the NWP fields have values which vary both horizontally and vertically.



(a) O3, CO, HCHO, Aerosol

The background error correlations and standard deviations for O3, CO, HCHO and aerosols were calculated using the National Meteorological Center (NMC) method (Parrish and Derber, 1992). For this, 150 days of 2-day IFS forecasts (CY47R1) were run, and differences between pairs of 24- and 48-hour forecast fields were calculated whose statistical characteristics serve as proxy for the background errors. The globally constant standard deviation at each model level is an average of the standard deviation for each grid point taken from the NMC statistics.

For the chemical species, O3, CO and HCHO, the background errors are directly calculated for each of the fields. For the total aerosol mixing ratio control variable, the background error standard deviations and correlations are for the total aerosol mass mixing ratio. The increment produced by the assimilation process for this total mass mixing ratio is repartitioned into the individual aerosol components according to their fractional contribution to the total aerosol mass (Benedetti *et al.*, 2009). This can lead to issues, which are documented in Flemming *et al.* (2017a).

(b) NO2, SO2, Volcanic SO2

The background error correlations for log(NO2), SO2 and Volcanic SO2 are prescribed analytical horizontal-only correlations. There are no vertical correlations between neighbouring levels. SO2 and Volcanic SO2 observations are currently only assimilated in the IFS-COMPO o-suite in the event of volcanic eruptions. An NMC or ensemble approach would not give useful SO2 background error statistics in these cases as the forecast model does not have information about individual volcanic eruptions, even though it does include emissions from outgassing volcanoes. Using an NMC ensemble approach for NO2 produces a lot of spurious long-range correlations that leads to a single observation of NO2 having an impact globally. This is not appropriate for a field that has very localised behaviour.

For all three fields the wavelet file is formed of diagonal vertical wavenumber correlation matrices, with the value on the diagonal controlled by a horizontal Gaussian correlation function. The values of the elements on the diagonal of each of these vertical correlation matrices are the same at every level but vary for each wavenumber as prescribed by the Gaussian correlation function. For SO2 and Volcanic SO2 the Gaussian correlation function has a lengthscale of 250km and for the log(NO2) variable it has a lengthscale of 200km. These lengthscales were chosen as they are a compromise between the wavelength that can be represented by the T95 and T159 inner loop grid resolutions of the IFS-COMPO configuration and the spread of the information from an observation.

In line with the control variable, the background error standard deviations for the log(NO2) variable are in log space. They are artificially curtailed to be practically zero in the stratosphere. This is because only tropospheric NO2 columns are assimilated and reducing the background standard deviation to close to zero constrains the influence of the observations to the troposphere in the assimilation process.

The background error standard deviations for SO2 and Volcanic SO2 are also artificially prescribed profiles. Calculating these using the NMC or ensemble methods will lead to peaks near the surface where anthropogenic SO2 concentrations are largest and will hence lead to the largest increments near the surface. This is not appropriate for volcanic eruptions which are generally elevated in the atmosphere. For the SO2 control variable, the background error standard deviation profile is a delta function that peaks in the mid troposphere around model level 98 (about 550hPA) in the 137 level model version. This corresponds to an SO2 plume height of about 5 km (Inness *et al.*, 2022). This delta function is used since the total column, volcanic-flagged observations of SO2 contain no information about the height of the SO2 plume. Constraining the background errors to be zero everywhere apart from the immediate vicinity of model level 98 forces the increment to be applied at this height. For the 'Volcanic SO2' control variable, which makes use of the altitude of the volcanic SO2 layer, the background error standard deviation profile is a constant in height and the SO2 observation operator defines a model equivalent to the observation by calculating a total column between the pressure values that correspond to the bottom and the top of the retrieved volcanic SO2 layer.



(c) CO2, CH4

The background error correlations and standard deviations for CO2 and CH4 were computed from a GHG EDA experiment (Massart and Bonavita, 2016). The EDA ensemble was preferred to a NMC ensemble method which was strongly impacted by model biases. In addition, a smoothing technique was applied to the horizontal correlations.

6.1.4 COMPO/GHG Observation operators

The observation operators provide the link between the analysis variables and the observations (Lorenc, 1986; Pailleux, 1990). The observation operator is applied to components of the model state to obtain the model equivalent of the observation, so that the model and observation can be compared like for like. The operator H in Eq. 6.1 above signifies the ensemble of all operators transforming the control variable x into the equivalent of each observed quantity, y^o , at observation locations. More information about the observation related processing in the IFS can be found in Part II Data assimilation, Chapter 5. Here, only observation operators dealing with atmospheric composition data are described further. Currently, only satellite retrievals of atmospheric composition are assimilated in the IFS-COMPO and IFS-GHG o-suites, and in-situ atmospheric composition data are only used for validation.

(a) Observation operators for chemical species

The satellite retrievals for the chemical species that are part of the control vector (O3, CO, NO2, SO2, HCHO) are total or partial column data, i.e. integrated layers bounded by a top and a bottom pressure. The model's background column value is either calculated as a simple vertical integral between the top and the bottom pressure of the partial or total column, or it is determined by applying the averaging kernels of the retrievals, at the time and location of the observation. The column retrievals can be written using the averaging kernel $\bf A$, that relates the true vertical profile $\bf x_t$ to the retrieved columns $\bf y^o$ as

$$\mathbf{y}^{o} = \mathbf{x}_{ap} + \mathbf{A}(\mathbf{x}_{t} - \mathbf{x}_{ap}) + \epsilon \tag{6.5}$$

where x_{ap} is an a-priori profile used in the retrieval of y^o and ffl an error term for measurement errors and errors in the forward model. In the observation operator we apply the averaging kernels A to the model profiles, x_m , to smooth the model profiles according to the sensitivity of the retrievals. This means Eq. 6.3 can be written as

$$\mathbf{d} = \mathbf{x}_{ap} + \mathbf{A}(\mathbf{x}_{t} - \mathbf{x}_{ap}) + \epsilon = \mathbf{A}(\mathbf{x}_{t} - \mathbf{\hat{H}}(\mathbf{x}_{m}))$$
(6.6)

where $\hat{\mathbf{H}}$ is an operator to calculate layer values of the chemical species from the model profiles on the vertical grid of the a-priori profile. Using this observation operator, we remove the explicit influence of the a-priori profile in the calculation of the departures, but knowledge of the a-priori profile is still needed in the observation operator calculations. Also, the impact of the a-priori remains implicitly through the dependence of the retrieval \mathbf{y}^o and the retrieval error on the a-priori, since a badly chosen a-priori will generally lead to larger retrieval errors and larger departures.

The master routine controlling the calls to the individual observation operators is called HOP and it calls the routine OBSOP_COMPOSITON which in turn calls the various observation operators for atmospheric composition data. Most chemical species are treated in the routine GRG_AK_OP (and the corresponding tangent-linear and adjoint routines GRG_AK_TL and GRG_AK_AD) where averaging kernels are applied to calculate the model equivalent of the observations. MOPITT CO data are treated separately in the routine MOPITT_AK_OP (and the corresponding tangent-linear and adjoint routines MOPITT_AK_TL and MOPITT_AK_AD) because the MOPITT averaging kernels work in log(VMR) space and a modified observation operator is required. There is a further routine MOPITT_PROFILE_AK (and the corresponding tangent-linear and adjoint routines MOPITT_PROFILE_AK_TL and MOPITT_PROFILE_AK_AD) that deals with MOPITT profile retrievals. However, in the operational IFS-COMPO o-suite only MOPITT total column CO data (from the thermal infrared (TIR) retrieval) are assimilated. For some chemical species (currently O3 and SO2) no averaging kernels are applied and the model equivalent of the observation is calculated as a simple vertical



integral between the top and bottom pressure values of the layer. This uses the routine PPNEW. There is also an observation operator to facilitate the assimilation of in-situ atmospheric composition data, for example IAGOS aircraft data. These data are currently not assimilated in the IFS-COMPO o-suite, but the relevant routines ISAC_GRG (and the corresponding tangent-linear and adjoint routines ISAC_GRGTL and ISAC_GRGAD) are in place and are also called from OBSOB_COMPOSTION.

(b) Observation operators for aerosols

The satellite retrievals used for aerosols are of Aerosol Optical Depth (AOD). The observation operator for AOD is based on precomputed optical properties (mass extinction coefficient, α_e , single scattering albedo, ω , and asymmetry parameter, g) for each of the aerosol species at each of the MODIS wavelengths λ (see Section 5.1.2 for full details of how the optical properties are calculated). The aerosols are assumed to be externally mixed. That is, the individual species are assumed to coexist in the volume of air considered and to retain their individual optical and chemical characteristics.

For the calculation of the model equivalent optical depth, the relative humidity (RH) is first computed from the model temperature, pressure and specific humidity. The appropriate mass extinction coefficients are then retrieved from the look-up table for the wavelength of interest (550nm as standard), multiplied by the aerosol mass mixing ratio which has been previously interpolated at the observation locations, and then integrated vertically. The total optical depth is the sum of the single-species optical depths as given by

$$\tau_{\lambda} = \sum_{i=1}^{N} \int_{p_{surf}}^{0} \alpha_{ei}(\lambda, RH(p)) r_i(p) \frac{dp}{g}, \tag{6.7}$$

where r is the mass mixing ratio, dp is the pressure of the model layer and g is the constant of gravity; p_{surf} represents the surface pressure. The number of aerosol species included in the calculation is given by N. The SO2 and Volcanic SO2 precursors are excluded from this calculation as they are not visible in the AOD observations.

The aerosol observation operator routine AOD_OP and the corresponding tangent-linear and adjoint routines AOD_TL and AOD_AD are all called from OBSOP_COMPOSITION.

6.2 COMPO/GHG ASSIMILATED OBSERVATION

More background information regarding the general treatment of observations in the IFS can be found in Part I Observations.

6.2.1 Observation data sets assimilated in the IFS-COMPO and IFS-GHG o-suites

Table 6.1 lists the satellite retrievals that have been assimilated in the IFS-COMPO o-suite between September 2014 and July 2022 and those assimilated in the (pre-operational) IFS-GHG o-suite since September 2021.



Table 6.1 Satellite retrievals of reactive, greenhouse gases and aerosol optical depth that are actively assimilated in the IFS-COMPO and IFS-GHG o-suites up to Cy48R1.

Instrument	Satellite	Provider	Version	Type	Status
MLS	AURA	NASA	V4	O ₃ profiles	20130107 - 20220207
			V5		20220207 - 20230216
			V5-NN		20230216 -
OMI	AURA	NASA	V883	O ₃ total column	20090901 -
GOME-2	Metop-A	EUMETSAT	GDP 4.8	O ₃ total column	20131007 - 20181231
GOME-2	Metop-B	EUMETSAT	GDP 4.8	O ₃ total column	20140512 -
GOME-2	Metop-C	EUMETSAT	GDP 4.9	O ₃ total column	20200505 -
SBUV-2	NOAA-19	NOAA	V8	O ₃ 21-layer profiles	20121007 - 20201005
OMPS	Suomi-NPP	NOAA / EUMETSAT		O ₃ 13-layer profiles	20170124 - 20190409 20201006 -
OMPS	NOAA-20	NOAA / EUMETSAT		O ₃ 13-layer profiles	20201006 - 20201215
0 1 1 2 0	- 1 - 1 - 1 - 1			-3y p	20230201 -
TROPOMI	Sentinel-5P	ESA		O ₃ column	20181204 -
IASI	MetOp-A	LATMOS/ULB EUMETSAT		CO total column	20090901 - 20180621
11.101	metop 11	Zimico, eza zemziani		Co total column	20180622 - 20191118
IASI	MetOp-B	LATMOS/ULB EUMETSAT		CO total column	20140918 - 20180621
	- Torret				20180622 -
IASI	MetOp-C	EUMETSAT		CO total column	20191119 -
MOPITT	TERRA	NCAR	V5-TIR	CO total column	20130129 -
			V7-TIR		20160124 - 20180626
			V7-TIR Lance		20180626 -
			V8-TIR		20190702 - 20211009
			V9-TIR		20211010 -
TROPOMI	Sentinel-5P	ESA		CO total column	20230627 -
OMI	AURA	KNMI	DOMINO V2.0	NO ₂ tropospheric column	20120705 - 20210331
GOME-2	MetOp-A	EUMETSAT	GDP 4.8	NO ₂ tropospheric column	20180626 - 20200504
GOME-2	MetOp-B	EUMETSAT	GDP 4.8	NO ₂ tropospheric column	20180626 -
GOME-2	MetOp-C	EUMETSAT	GDP 4.9	NO ₂ tropospheric column	20200505 -
TROPOMI	Sentinel-5P	ESA	v2.2.0/v2.3.1	NO ₂ tropospheric column	20211013 -
GOME-2	MetOp-A	EUMETSAT	GDP 4.8	SO ₂ total column	20150902 - 20191210
GOME-2	MetOp-B	EUMETSAT	GDP 4.8	SO ₂ total column	20150902 -
GOME-2	MetOp-C	EUMETSAT	GDP 4.9	SO ₂ total column	20200505 -
TROPOMI	Sentinel-5P	ESA		Volcanic SO ₂ total column	20201006 -
MODIS	AQUA	NASA	Col. 5 Deep Blue	Aerosol optical depth	20090901 -
	TERRA		Col. 6, 6.1	Fire radiative power	20150902 -
				_	20170124 -
VIIRS	SNPP NOAA-20	NASA	V3r0	Aerosol optical depth	20230201 -
PMAp	METOP-A	EUMETSAT		Aerosol Optical Depth	20170124 - 20210719
т	METOP-B				20170926 -
	METOP-C				20210719 -
IASI	METOP-B	LMD	v4.0	CO2 mid-tropospheric col-	20210901 - 20220712
			v10.1	umn	20220712 -
IASI	METOP-B	LMD	v8.1	CH4 mid-tropospheric col-	20210901 - 20220715
			v10.1	umn	20220715 -
TANSO	GOSAT-1	IUP-UB	BESD	CO2 total column	20210901 - 20220621
			FOCAL v3.0		20220621-
TANSO	GOSAT-1	SRON	Proxy/SRPR	CH4 total column	20210901 - 20220711
			Full Physics v2.3.8		20220711 -

6.2.2 Quality control (variational quality control, first-guess check, blacklisting) and observation errors

The observation error and background error covariance matrices determine the relative weight given to the observation and the background in the analysis (see Eq. 6.1). For the chemical species, observation errors as given by the data providers are used. If the error values for species other than CO2 and CH4 are below 5 %, a minimum value of 5% is taken. The observation errors in both the IFS-COMPO and IFS-GHG o-suites are assumed to include any observation operator errors and representativeness errors that could arise because of differences in resolution of observation and the model, and that accounts for scales unresolved by the model. The observation errors for both COMPO and GHG species are given in the observation BUFR files and are further modified for some species in the routine REO3SIN. The screening processes to determine if an observation will be used in the analysis happen in the first trajectory run of each analysis cycle. They include the data selection criteria defined in the blocklist (formerly blacklist) as well as first-guess checks, variational quality control and data thinning. Most data selection criteria are coded in so called blocklist files, written in a convenient, readable blocklist language (see the Blocklist Documentation; Järvinen *et al.* (1996)). The blocklist mechanism is very flexible and allows





Figure 6.1 Timeseries of satellite retrievals assimilated in the IFS-COMPO o-suite since 2014. Green lines show observations for which averaging kernels are used. The numbers to the right of the plot list the reportypes that are used to identify the data in the observational data base (ODB), see https://apps.ecmwf.int/odbgov/all/ for more information.

nearly complete control of which data to use/not use in the assimilation. The observations are scanned through for blocklisting in the subroutine BLACK. At the set-up stage the blocklist interface is initialised (BLINIT) to the external blocklist library. The blocklist files consist formally of two parts. Firstly, the selection of variables for assimilation is specified in the 'data selection' part of the blocklist. This controls which observation types, variables, vertical ranges etc. will be selected for the assimilation. Some more complicated decisions are also performed through the data selection file; for instance, an orographic rejection limit is applied in the case of the observation being too deep inside the model orography; data might be temporarily blocklisted because of algorithm upgrades. This part of the blocklist also provides a handy tool for experimentation with the observing system, as well as with the assimilation system itself. Secondly, a 'monthly monitoring' blocklist is provided for discarding the stations that have recently been reporting in an excessively noisy or biased manner compared with the ECMWF background field. This 'monthly blocklist' is maintained by the Forecast Department. Depending on the blocklisting criteria, flags are communicated to the routine BLACK, and those are written to the ECMA ODB data base. Blocklist-rejected data are subsequently excluded from the CCMA ODB and will not be present in the 4DVAR minimisation job steps. The operational blocklist history is kept in an archive.

Currently (CY48R1), the IFS-COMPO o-suite maintains its own copy of the operational blocklist, with a dedicated part containing blocklist criteria for the chemical species and aerosols, as well as the deactivation of IR ozone channels from AIRS, IASI, HIRS and CriS that are used in the ECMWF NWP system but not used by in the IFS-COMPO configuration. The IFS-GHG o-suite uses the operational NWP blocklist and adds a section for CO2 and CH4 observations. This happens in the script ADD-CAMS_BLACK.

Variational quality control (VarQC) and background error checks are carried out for the atmospheric composition data. General information about background quality control can be found in https://www.ecmwf.int/en/elibrary/19745-ifs-documentation-cy47r1-part-ii-observations and about VarQC in https://www.ecmwf.int/en/elibrary/19746-ifs-documentation-cy47r1-part-ii-data-assimilation. Here we only highlight some of the points that apply to the atmospheric composition data, with more details given for specific species when necessary. The variational quality control, VarQC, has been described by Andersson and Järvinen (1999). It is a quality control mechanism which is



incorporated within the variational analysis itself. A modification of the observation cost function to take into account the non-Gaussian nature of gross errors has the effect of reducing the analysis weight given to data with large departures from the current iterant (or preliminary analysis). Data are not irrevocably rejected but can regain influence on the analysis during later iterations if supported by surrounding data.

The switch LVARQC in DEFRUN (can be modified via the namelist NAMJO) determines if VarQC is carried out for a variable. VarQC is currently carried out for all atmospheric composition control variables except for SO2 in the IFS-COMPO configuration. Only volcanic SO2 observations are assimilated in the IFS-COMPO o-suite and these usually deviate a lot from the background SO2 values which do not include information about the volcanic eruption. (In a way the volcanic SO2 data are used as a source to bring the information about a volcanic eruption into the model.) Therefore, these observations will have large first-guess departures but should not be rejected or given reduced weight by the VarQC.

All observations are assigned an estimate of the background error in observation space for later use in the background quality control, and this estimate is stored in the ODB under fg_error. This estimate is only used to determine the expected variance of the background departures in the quality control against the background, and it is technically separate from the background error used during the assimilation for the control variables to determine the weighting of observations. In the routine FGCHK first-guess errors are set to 20% of the first-guess values for AOD and the chemical species, to 1% of the firstguess value for CO2 and to 2% of the first-guess value for CH4. The background quality control (FIRST) is performed for the variables that are intended to be used in the assimilation. The procedure is as follows. The variance of the background departure $y^{o} - Hx^{b}$ can be estimated as a sum of observation and background-error variances $\mathbf{e}_{o}^{2} + \mathbf{e}_{b}^{2}$, assuming that the observation and the background errors are uncorrelated. After normalising with $\mathbf{\alpha}_{b}$, the estimate of variance for the normalised departure is given by $1 + (\mathbf{e}_0^2)/\mathbf{e}_b^2$. In the background quality control, the square of the normalised background departure is considered as suspect when it exceeds its expected variance by more than a predefined multiple (FGCHK, SUFGLIM). These predefined limits (RBGQC) are set in DEFRUN and can be changed in namelist NAMIO. For the chemical species these factors currently are {9, 16, 25}; for aerosols {4, 9, 16}; while for GHG they depend on the species: they are {9, 16, 25} for CO2 and {2.25, 4, 9} for CH4. These values are also the default values used in the variational quality control to determine which observations are either rejected or given less weight. The RBGQC values mean that, e.g. for the chemical species, an observation is rejected if the square of the normalised background departure is greater than 5 and given reduced weight if it is greater than 3. No first-guess check is carried out for SO2, again because the volcanic SO2 data will per se be showing large differences from the model background.

6.2.3 Bias correction and anchoring

Retrievals of the same parameter from different satellite instruments can have biases with respect to each other or to the model. Assimilating biased data violates one of the underlying assumptions of data assimilation, namely that the data should be unbiased, and therefore a bias correction scheme has to be applied to the data. Variational bias correction (VarBC, Dee (2004)) of observations was first introduced into the IFS in Cy31r1. VarBC works by including additional degrees of freedom (bias parameters) in the observational term of the 4D-Var cost function to account for possible systematic errors in selected observations and/or observation operators. The systematic errors (or biases) are represented by linear predictor models, which can be formulated separately for different groups of observations. More information about the general working of VarBC can be found in Part II Data assimilation, Chapter 5. VarBC is applied to several of the atmospheric composition data assimilated in the IFS-COMPO o-suite (see Table 6.2). Table 6.2 also lists the predictors used for the various instruments. Some data sets are used to 'anchor' the bias correction for a chemical species, i.e. are assimilated without bias correction. Past experience had shown that it is important to have such anchors for the bias correction to avoid drifts in the fields (Inness et al., 2013). The VarBC settings for the atmospheric composition data are defined in the routine VARBC_TO3 and can be modified via the namelist NAMVARBC_TO3 in the scripts IFSTRAJ, IFSMIN or OOPSVAR. The predictors available for use in VarBC are defined in the routine VARBC_PRED.



Table 6.2 *Variational Bias correction information for atmospheric composition data used in the IFS-COMPO osuite (CY48R1). SOE denotes solar elevation. Thermal contrast is the temperature difference between the surface and the lowest model level. No bias correction is currently applied to GHG observations.*

Species	Satellite	Instrument	VarBC	Predictors
			applied	
O3	Metop-B	GOME-2	yes	Constant, SOE
O3	Metop-C	GOME-2	yes	Constant, SOE
O3	Aura	OMI	yes	Constant, SOE
O3	Sentinel-5p	TROPOMI	yes	Constant, SOE
O3	SNPP	OMPS	yes	Constant, SOE
O3	NOAA-20	OMPS	yes	Constant, SOE
O3	Aura	MLS	no	
CO	Terra	MOPITT	yes	Constant, 1000-300 hPa thickness, ther-
				mal contrast
CO	Metop-B	IASI	yes	Constant, 1000-300 hPa thickness, ther-
				mal contrast
CO	Metop-C	IASI	no	
CO	Sentinel-5p	TROPOMI	no	
NO2	Metop-B	GOME-2	yes	Constant, SOE
NO2	Metop-C	GOME-2	no	
NO2	Sentinel-5p	TROPOMI	no	
SO2 (volcanic)	Metop-B	GOME-2	no	
SO2 (volcanic)	Metop-C	GOME-2	no	
SO2 (volcanic)	Sentinel-5p	TROPOMI	no	
AOD	Aqua	MODIS	yes	Constant, surface wind over sea
AOD	Terra	MODIS	yes	Constant, surface wind over sea
AOD	SNPP	VIIRS	yes	Constant, surface wind over sea
AOD	NOAA-20	VIIRS	no	
AOD	METOP-B	PMAp	yes	Constant, surface wind over sea
AOD	METOP-C	PMAp	yes	Constant, surface wind over sea

6.2.4 Data thinning and super-obbing

Thinning of the atmospheric composition data is carried out in several places. First, there is the so-called pre-screening (carried out in the prepare_obs tasks under the obs family). Any data thinned here are discarded, i.e. not included in the ODB, and will not be available for use (either actively or passively) in the analysis. For atmospheric composition data this pre-screening happens in the task PREROE3 and uses the routine satrad/programs/REO3_PRESCREEN.

Alternatively, observation numbers can be reduced by averaging data to so-called super-observations. This happens in the task PREREO3_SUPEROB and is currently applied to TROPOMI and VIIRS data. The super-obbing uses the routines satrad/programs/BUFR_GRID_SCREEN and satrad/programs/BUFR_SCREEN_REO3_SUPEROB.

In addition to the thinning in the pre-screening, data can also be thinned in the IFS (routine NEW_THINN_REO3). Data thinned here are included in the ODB as passive observations and therefore available for comparison against the model background. This thinning is controlled by settings in a file on the super computer \$XDATA_CAMS/\$IFS_CYCLE/sat/thin_reo3 (linked in the script MKLINKS). In CY48R1 the chemical species and aerosol data that are not super-obbed are thinned here to 0.5°. This is currently applied to O3 data from GOME-2 and OMI, CO data from IASI and MOPITT, NO2 data from GOME-2, AOD data from MODIS and PMAp. GHG observations are currently thinned to 1° x 1° applied to CH4 and CO2 from IASI and TANSO. This screening is done by randomly selecting an observation in the grid box (i.e. the first observation the thinning comes across).



6.3 TANGENT LINEAR AND ADJOINT REPRESENTATION OF ATMOSPHERIC COMPOSITION PROCESSES

The tangent linear (TL) and adjoint (AD) models for the chemical processes in the IFS are based on a simplified version of the forward chemical model. The simplified chemical model consists of two types of reactions, namely, the NO_x photochemical equilibrium and the production of nitric acid (HNO₃) from NO_2 oxidation (NO_x sink):

$$NO + O_3 \longrightarrow NO_2$$
 (6.8)

$$NO_2 + hv \longrightarrow NO + O_3$$
 (6.9)

$$NO_2 + OH \longrightarrow HNO_3$$
 (6.10)

Furthermore, in the reactions above, at each chemical time step, the concentrations of O_3 and OH are considered constant and are taken from the outer-loop trajectory computed in task IFSTRAJ. Therefore, at each time step, only increments in NO_2 and NO are propagated by the TL model during the minimisation (task IFSMIN), and, reciprocally, only adjoint forcings associated with NO_2 observations are propagated backward in time to the initial NO_2 and NO concentrations.

Starting from the main physics routines, the following routine calls implement the simplified chemistry TL/AD models:

- Tangent-linear integration: CALLPARTL>CHEM_MAIN_LAYER_TL>CHEM_MAIN_TL>CHEM_TM5_TL>TM5_O3CHEM_TL
- Adjoint integration: CALLPARAD>CHEM_MAIN_LAYER_AD>CHEM_MAIN_AD>CHEM_TM5_AD>TM5_O3CHEM_AD

The actual TL and AD codes associated with reactions 6.8 to 6.10 are implemented in TM5_O3CHEM_TL and TM5_O3CHEM_AD, respectively.

The chemistry TL/AD can be activated by setting LCHEM_TL=TRUE in prepIFS in the Atmospheric Composition section. It is activated by default in operation.



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