Coupling Convection with the Continuity Equation – a Multi-fluid approach

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11 July 2018

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Here is how to do it

Conditional Filtering [Thuburn et al., 2018]

Each location of the continuous fluid is given one of a number of labels, depending on the model complexity. Eg:

$$I_0(\mathbf{x},t) = \begin{cases} 1 & \text{if fluid is in stable atmosphere} \\ 0 & \text{otherwise} \end{cases}$$

$$I_1(\mathbf{x},t) = \begin{cases} 1 & \text{if fluid is in a buoyant plume} \\ 0 & \text{otherwise} \end{cases}$$

$$I_2(\mathbf{x},t) = \begin{cases} 1 & \text{if fluid is in a downdraft} \\ 0 & \text{otherwise} \end{cases}$$

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• Apply a spatial filter, for example averaging over grid boxes:

$$\sigma_i = \overline{I_i}$$

$$\rho_i = \overline{I_i\rho}$$

$$\rho_i \mathbf{u}_i = \overline{I_i\rho \mathbf{u}}$$

$$\rho_i \theta_i = \overline{I_i\rho \theta}$$

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$$\begin{aligned} \sigma_i &= \overline{I_i} \\ \rho_i &= \overline{I_i \rho} \\ \rho_i \mathbf{u}_i &= \overline{I_i \rho \mathbf{u}} \\ \rho_i \theta_i &= \overline{I_i \rho \theta} \end{aligned}$$

Derive equations of motion for each fluid and parametrise interactions

Conditionally Filter the Compressible Euler Equations

$$\frac{\partial \sigma_i \rho_i \mathbf{u}_i}{\partial t} + \nabla \cdot \left(\sigma_i \rho_i \mathbf{u}_i \mathbf{u}_i + \mathbf{F}_{\mathrm{SF}}^{\mathbf{u}_i} \right) + c_p \overline{I_i \rho \, \theta \nabla \pi} - \sigma_i \rho_i \mathbf{g} = \sum_{j \neq i} \left(\sigma_j \rho_j \mathbf{u}_j S_{ji} - \sigma_i \rho_i \mathbf{u}_i S_{ij} \right)$$
$$\frac{\partial \sigma_i \rho_i}{\partial t} + \nabla \cdot \left(\sigma_i \rho_i \mathbf{u}_i \right) = \sum_{j \neq i} \left(\sigma_j \rho_j S_{ji} - \sigma_i \rho_i S_{ij} \right)$$
$$\frac{\partial \sigma_i \rho_i \theta_i}{\partial t} + \nabla \cdot \left(\sigma_i \rho_i \mathbf{u}_i \theta_i + \mathbf{F}_{\mathrm{SF}}^{\theta_i} \right) = \sum_{j \neq i} \left(\sigma_j \rho_j \theta_j S_{ji} - \sigma_i \rho_i \theta_i S_{ij} \right)$$

Note sub-filter scale fluxes (due to non-linearities):

$$\overline{I_i \rho \mathbf{u} \theta} = \sigma_i \rho_i \mathbf{u}_i \theta_i + \mathbf{F}_{SF}^{\theta_i}$$

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Assume that pressure is uniform between fluids and that:

$$\overline{I_i \rho \theta \nabla \pi} = \sigma_i \rho_i \theta_i \nabla \pi + \sum_{j \neq i} \sigma_j \sigma_j \mathbf{d}_{ij} + \mathbf{F}_{\mathrm{SF}}^{\Pi_i}$$

- d_{ij} is drag exerted by fluid *j* on fluid *i*
- $\sigma_i \rho_i S_{ij}$ is mass transfer rate from fluid *i* to fluid *j*
- ► Straightforward to do the same for moisture variables

Advective Form

Need to solve in advective (or vector invariant) form to avoid problems when $\sigma_i \rightarrow 0$ and for bounded advection of σ_i . Ignoring sub-filter-scale fluxes:

$$\begin{aligned} \frac{\partial \mathbf{u}_i}{\partial t} + \mathbf{u}_i \cdot \nabla \mathbf{u}_i &= -2\Omega \times \mathbf{u}_i - c_p \theta_i \nabla \pi + \mathbf{g} + \sum_{j \neq i} \left(\frac{\sigma_j \rho_j}{\sigma_i \rho_i} S_{ji} (\mathbf{u}_j - \mathbf{u}_i) - \mathbf{D}_{ij} \right) \\ \frac{\partial \sigma_i \rho_i}{\partial t} + \nabla \cdot (\sigma_i \rho_i \mathbf{u}_i) &= \sum_{j \neq i} (\sigma_j \rho_j S_{ji} - \sigma_i \rho_i S_{ij}) \\ \frac{\partial \theta_i}{\partial t} + \mathbf{u}_i \cdot \nabla \theta_i &= \sum_{j \neq i} \left(\frac{\sigma_j \rho_j}{\sigma_i \rho_i} S_{ji} (\theta_j - \theta_i) \right) \end{aligned}$$

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Equation of State $p_0 \pi^{\frac{1-\kappa}{\kappa}} = R \rho_i \theta_i = R \rho \theta = R \sum_i \sigma_i \rho_i \theta_i$

Numerical Solution [Weller and McIntyre, submitted]

- Finite Volume Advection
 - Bounded advection of $\sigma_i \rho_i$ (TVD scheme with van-Leer limiter)
 - θ_i and \mathbf{u}_i advected using using flux form operators:

$$\mathbf{u}_i \cdot \nabla \boldsymbol{\theta}_i = \nabla \cdot (\boldsymbol{\theta}_i \mathbf{u}_i) - \boldsymbol{\theta}_i \nabla \cdot \mathbf{u}_i$$

- Lorenz C-grid staggering
- Semi-implict: implicit acoustic waves
 - Velocity and density in each fluid expressed as a function of Exner pressure, π
 - Substituted into continuity equation to get Helmholtz equation for π

Rising Bubble, two fluids with different initial conditions

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- No transfer terms, stabilisation or sub-filter fluxes
- Two initially hydrostatically balanced, stationary fluids
- Fluid 0 (stable fluid):
 - $\theta_0 = 300 \text{K}$ • $\sigma_0 = \begin{cases} 0.5 & \text{circle near the ground} \\ 1 & \text{elsewhere} \end{cases}$
- Fluid 1 (buoyant fluid):
 - $\bullet \quad \theta_1 = \begin{cases} 300\text{K} + \theta' & \text{in circle} \\ 300\text{K} & \text{elsewhere} \end{cases}$ $\bullet \quad \sigma_1 = \begin{cases} 0.5 & \text{circle near the ground} \\ 0 & \text{elsewhere} \end{cases}$

► If we ignore sub-filter scale fluxes, drag and mass transfers then these equations are ill posed [Stewart and Wendroff, 1984]

Effective stabilisation options:

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Diffusion between fluids (diffuse σ_i) Weller and McIntyre [submitted]

$$\sigma_i \rho_i S_{ij} = \frac{K_{\sigma}}{2} \max \left(\nabla^2 \left(\sigma_j \rho_j - \sigma_i \rho_i \right), 0 \right)$$

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Drag between fluids

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Remove divergence local to just one fluid: Weller and McIntyre [submitted]

$$\sigma_i \rho_i S_{ij} = \frac{1}{2} \max \left(\sigma_j \rho_j \nabla \cdot \mathbf{u}_j - \sigma_i \rho_i \nabla \cdot \mathbf{u}_i, 0 \right)$$

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leads to a bounded transport equation for σ_i

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$$\mathbf{D}_{ij} = \frac{\sigma_j}{\rho_i} \frac{C_D \overline{\rho}}{r_c} |\mathbf{u}_i - \mathbf{u}_j| (\mathbf{u}_i - \mathbf{u}_j)$$

▶ Remove divergence local to just one fluid: Weller and McIntyre [submitted]

$$\sigma_i \rho_i S_{ij} = \frac{1}{2} \max \left(\sigma_j \rho_j \nabla \cdot \mathbf{u}_j - \sigma_i \rho_i \nabla \cdot \mathbf{u}_i, 0 \right)$$

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leads to a bounded transport equation for σ_i

Diffusion of vertical velocity (a sub-filter-scale flux) (John Thuburn)

Stabilisation by removing divergence local to one fluid

Continuity equation:

$$\frac{\partial \sigma_i \rho_i}{\partial t} + \nabla \cdot (\sigma_i \rho_i \mathbf{u}_i) = \sum_{j \neq i} (\sigma_j \rho_j S_{ji} - \sigma_i \rho_i S_{ij})$$

Transfer converging fluid:

$$\sigma_i \rho_i S_{ij} = \frac{1}{2} \max \left(\sigma_j \rho_j \nabla \cdot \mathbf{u}_j - \sigma_i \rho_i \nabla \cdot \mathbf{u}_i, 0 \right)$$

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leads to a bounded transport equation for σ_i

$$\frac{\partial \sigma_i \rho_i}{\partial t} + \mathbf{u}_i \cdot \nabla(\sigma_i \rho_i) = -\frac{1}{2} \overline{\rho \nabla \cdot \mathbf{u}}$$

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The transfer terms can be large :..

- Operator splitting to ensure boundedness
- Implicit treatment for stability $(\frac{\sigma_i \rho_j}{\sigma_i \rho_i} S_{ji} \rightarrow \infty \text{ as } \sigma_i \rho_i \rightarrow 0)$

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 For example for θ_i:

Advection:
$$\theta_i' = \theta_i^n - \Delta t \left\{ (1 - \alpha) \mathbf{u}_i^n \cdot \nabla \theta_i^n + \alpha \mathbf{u}_i' \cdot \nabla \theta_i' \right\}$$

Transfers: $\theta_i^{n+1} = \theta_i' + \Delta t \sum_{j \neq i} \frac{\sigma_j \rho_j}{\sigma_i \rho_i} S_{ji} \left(\theta_i^{n+1} - \theta_j^{n+1} \right)$

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Shorthand: $T_{ij} = \Delta t \frac{\sigma_j \rho_j}{\sigma_i \rho_i} S_{ji}$ and re-arrange for i = 0, 1, 2:

$$\begin{pmatrix} 1+T_{01}+T_{02} & -T_{01} & -T_{02} \\ -T_{10} & 1+T_{10}+T_{12} & -T_{12} \\ -T_{20} & -T_{21} & 1+T_{21}+T_{21} \end{pmatrix} \begin{pmatrix} \theta_0^{n+1} \\ \theta_1^{n+1} \\ \theta_2^{n+1} \end{pmatrix} = \begin{pmatrix} \theta_0' \\ \theta_1' \\ \theta_2' \end{pmatrix}$$

Drag Between Fluids

From formula for drag on a rising bubble

$$D_{ij} = \sigma_j \frac{C_D}{r_c} \frac{\bar{\rho}}{\rho_i} |\mathbf{u}_i - \mathbf{u}_j| (\mathbf{u}_i - \mathbf{u}_j)$$

 r_c = bubble or plume radius. As σ_i becomes small we need r_c to become small so that the drag is large and the vanishing fluid moves with the mean flow:

$$r_{c} = \max\left(r_{\min}, r_{\max}\prod_{i}\sigma_{i}\right) \quad (1)$$

Try $C_{D} = 1, r_{\min} = 100m, r_{\max} = 2000m$

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Diffusion Between Fluids

- Similar to convective entrainment
- Diffusion coefficient, K_σ, could be chosen based on wind shear

$$\sigma_i \rho_i S_{ij} = \frac{K_{\sigma}}{2} \max \left(\nabla^2 \left(\sigma_j \rho_j - \sigma_i \rho_i \right), 0 \right)$$

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- Total mass is not diffused
- Will control oscillations in σ
- Try $K_{\sigma} = 200 \text{ m}^2 \text{s}^{-1}$

Transfer Converging Fluid

- Removes divergence that is local to one fluid
- Equation for σ_i becomes bounded
- $\bullet \ \boldsymbol{\sigma}_i \boldsymbol{\rho}_i \boldsymbol{S}_{ij} = \frac{1}{2} \max \left(\boldsymbol{\sigma}_j \boldsymbol{\rho}_j \nabla \cdot \mathbf{u}_j \boldsymbol{\sigma}_i \boldsymbol{\rho}_i \nabla \cdot \mathbf{u}_i, \ 0 \right)$

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No arbitrary coefficients

Mass Transfer based on Buoyancy Perturbations for Convection

- Positive θ₀ anomalies should be transferred to fluid one
- Write this in terms of PDEs
- How do we diagnose this without using a reference state?

$$S_{01} = \begin{cases} -K_{\theta} \frac{\nabla^2 \theta_0}{\theta_0} & \text{when } \nabla^2 \theta_0 < 0\\ 0 & \text{otherwise} \end{cases}$$
$$S_{10} = \begin{cases} K_{\theta} \frac{\nabla^2 \theta_1}{\theta_1} & \text{when } \nabla^2 \theta_1 > 0\\ 0 & \text{otherwise} \end{cases}$$

- Divergence transfer to stabilise
- Simulation using $\sigma_0 = 0$ everywhere initially
- Warm anomaly initially in fluid 0
- $K_{\theta} = 10^6 \text{ m}^2 \text{s}^{-1}$

Conclusions

Stable numerical method for solving advective form multi-fluid equations

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- Forms of stabilisation:
 - Diffusion of mass between fluids
 - Drag between fluids
 - Transfer converging fluid no parameters to set
- To mimic convective parameterisation, transfer based on $\nabla^2 \theta_i$

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