# Pedotransfer Functions for Permeability: A Computational Study at Pore Scales

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Abstract. Three phenomenological power law models for the permeabil-3 ity of porous media are derived from computational experiments with flow 4 through explicit pore spaces. The pore spaces are represented by three di-5 nensional pore networks in sixty-three virtual porous media along with fif-6 teen physical pore networks. The power laws relate permeability to (i) poros-7 ity, (ii) squared mean hydraulic radius of pores, and (iii) their product. Their 8 performance is compared to estimate derived via the Kozeny equation, which 9 also uses the product of porosity with squared mean hydraulic pore radius 10 to estimate permeability. The power laws provide tighter estimates than the 11 Kozeny equation even after adjusting for the extra parameter they each re-12 quire. The best fit is with the power law based on the Kozeny predictor, that 13 is, the product of porosity with the square of mean hydraulic pore radius. 14

### 1. Introduction

Flows of fluid through a porous medium are distinguished from flows through open 15 bodies by spatially variable resistance arising from variations in the medium's pore space 16 geometry and topology that yields a steady flow. At pore-resolving scales a porous medium 17 is a network of explicit, interconnected channels embedded in a solid medium. Critical 18 parameters affecting resistance in pore spaces include typical radius of the pores, the 19 length of a streamline between two points relative to the distance between the points, 20 and the density of pores. Sample volumes ranging from 0.01-1000 cm<sup>3</sup> are typical of 21 laboratory pore space experiments with most at the lower end of the range. At macroscopic 22 scales, porous media are usually represented as volumes with system states, e.g. velocity 23 and hydraulic head, and parameters, e.g. permeability and porosity, defined piece-wise 24 continuously at every point in the volume. Macroscopic resistance to flow is quantified 25 by its approximate inverse, permeability, which is defined via Darcy's law in terms of the 26 ratio of fluid flux to the gradient of pressure within the fluid. Darcy's law was established 27 experimentally [Darcy, 1856] and later derived analytically by upscaling pore-network 28 flows through homogenization, or volume averaging [Shvidler, 1964; Whitaker, 1999]. 29 Alternatives based on ensemble averaging have also been used to estimate permeability 30 from pore-scale properties of porous media [Rubinstein, 1986]. 31

Although permeability is a well-established property of most relatively uniform porous media, its actual dependence on specific geometric and topological properties of porous networks is not fully understood. Phenomenological transfer functions have been developed by soil physicists, hydrologists, chemical and petroleum engineers, and materials

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scientists to estimate permeability from properties of porous media that are relatively easy to observe. A natural starting point is to suppose that a sample volume's permeability is proportional to its porosity since the latter indicates pore density and is a good measure of the medium's capacity to hold fluid. Yet this is not entirely satisfactory, since two porous media can have the same porosity but one may be entirely impermeable while the other offers minimal resistance to flow.

Perhaps the best known phenomenological transfer functions are the Kozeny equation [Kozeny, 1932; Carman, 1956; Bear, 1988] and the Kozeny-Carman equation [Carman, 1939]. Kozeny derived his equation,

$$k = c_0 n R^2, \tag{1}$$

by reasoning about flow through an idealized pore network: he equated the velocity given 46 by Poiseuille's law for flow through a bundle of capillary tubes to the specific discharge 47 obtained from Darcy's law and thus solved for permeability. He concluded that perme-48 ability, k, is proportional to the product of porosity, n, with the square of mean hydraulic 49 radius, R, a measure of typical pore size. Hence, the Kozeny predictor,  $nR^2$ , combines a 50 factor, n, depending on the capacity of a medium to hold fluid with another, R, depending 51 on the ability of the medium to transmit it. The dimensionless constant,  $c_0$ , is known as 52 the Kozeny coefficient. Carman [1939] extended (1) by including a factor of tortuosity,  $\tau$ , 53 an index of the complexity of streamlines in the medium, and derived the Kozeny-Carman 54 equation 55

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$$k = c_0' n R^2 / \tau^2.$$
 (2)

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Since permeability is a characteristic of a porous medium, (1) and (2) need to be properly scaled by fluid viscosity and density to relate a medium's permeability to its saturated hydraulic conductivity with respect to a particular fluid.

We follow Smolarkiewicz and Winter [2010], [SW10] for brevity, and determine per-60 meability computationally by simulating the basic elements of Darcy's original experi-61 ment [Darcy, 1856] in three-dimensional networks of pores, allowing pore-scale processes 62 to be observed in detail. Hyman et al. [2012], hereafter [HSW12], employed the techniques 63 of [SW10] to study the influence of porosity on the degree of heterogeneity in steady state 64 flows within stochastically generated three dimensional pore networks. [HSW12] reports 65 technical aspects of modeling flow in explicit pore spaces and provides a Lagrangian per-66 spective of the pore space via particle tracking. That paper focuses on heterogeneity of 67 microscopic flow field and its relationship to porosity, while this paper focuses on the 68 continuum scale properties of permeability. They quantify the degree of heterogeneity in 69 the flow and identify coherent heterogeneities in the flow field by tracking fluid particles 70 and recording various attributes including tortuosity, trajectory length, and first passage 71 time in media with porosities between 0.2 and 0.7. 72

Here, the techniques of [SW10] are used to estimate overall permeability for each of seventy-eight small,  $O(1 \text{ cm}^3)$ , sample volumes of porous media. Sixty-three realizations are drawn from ensembles of virtual pore spaces with porosities ranging from 0.19 to 0.84, while the others are a volcanic tuff [*Wildenschild et al.*, 2004], a column of glass beads [*Culligan et al.*, 2004], and thirteen unique sandpacks, sandstones, and carbonate from *Mostaghimi et al.* [2013]. Virtual pore spaces are isotropic and statistically stationary in space with permeabilities corresponding to a well-sorted gravel or sand [*SW10*];

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<sup>80</sup> [*HSW12*] demonstrated that the virtual media are large enough to constitute representa-<sup>81</sup> tive elementary volumes. Their material properties appear consistent with those of the <sup>82</sup> glass beads and tuff. Owing to the high resolution of the seventy-eight pore space samples, <sup>83</sup> porosity and hydraulic radius can be directly evaluated.

The computed permeability, porosity, and hydraulic radii of the virtual media are used 84 to empirically estimate the Kozeny coefficient,  $c_0$ . The estimate  $\hat{c}_0 = 0.19$  is in excellent 85 agreement with Carman's original value,  $c_0 = 0.2$ , indicating the representativeness of the 86 virtual pore spaces. Additionally, over a restricted range of porosities, 0.2 < n < 0.7, the 87 analytically derived Kozeny and Kozeny-Carman laws are both reproduced reasonably 88 well. The Kozeny equation (1) fits results from media with porosities in 0.2 < n < 0.789 fairly well and the Kozeny coefficient is within an interval later noted by noted by Carman 90 [1956]. The Kozeny-Carman equation (2) also predicts permeability adequately within this 91 limited range and the computed coefficient,  $c'_0$ , is near that suggested by Carman. 92

Yet the Kozeny equation is not entirely satisfactory as a predictor of permeability for 93 the entire data set. Plotting the permeability data against the Kozeny predictor,  $nR^2$ , 94 reveals an obvious nonlinearity at large and small values of  $nR^2$  that is not captured by 95 the linear (in the predictor) Kozeny model. Hence, scale-invariant power law alternatives 96 depending upon porosity, n, the square of hydraulic radius, R, and the Kozeny predictor, 97  $nR^2$ , that is their product, are derived and compared to the Kozeny equation. Focus is 98 placed on the Kozeny equation and related power laws rather than the Kozeny-Carman 99 equation because the tortuosity of the data is highly correlated with porosity and mean 100 hydraulic radius. 101

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The power law alternatives provide better fits to the physical and virtual data, although 102 at the expense of adding an extra parameter, than does the Kozeny equation over the 103 entire range of data. We attribute this to the ability of simple power laws to capture the 104 nonlinear effects of pore space interconnectivity on permeability at extremes of porosity 105 and mean hydraulic radius. This seems born out by a power law based on the Kozeny 106 predictor,  $nR^2$ , which yields a sum of squared errors for the virtual data that is significantly 107 smaller than the errors of power laws based on porosity or mean hydraulic radius alone. 108 Goodness of fit and model performance for these data are evaluated using a standard 109 statistical technique, the Analysis of Variance, to gauge the relative advantage conferred 110 by the additional parameter. The overall fit of the models to both real and synthetic data 111 is evaluated and compared using chi-squared tests. 112

Section 2 reviews previous studies to determine permeability computationally and places 113 the present work within context of the previous studies. Section 3 describes simulations of 114 pore networks and flow; computational methods for generating virtual porous media along 115 with a characterization of the physical data (Section 3.1), numerical techniques for resolv-116 ing flow in the explicit pore networks (Section 3.2), and estimation of transfer function 117 variables including porosity, hydraulic radius, tortuosity, and permeability (Section 3.3-118 3.4). A preliminary study to determine a proper grid resolution for the study is performed 119 prior to derivations of the power law alternatives to the Kozeny equation (Section 3.5). 120 Next the empirical pedotransfer functions are derived and evaluated (Section 4.1), and 121 their ranges of applicability are discussed (Section 4.2). We finish with a summary of the 122 experiment and offer a few remarks about the generality of the results in Section 5. 123

## 2. Background

Pedotransfer functions are mathematical or computational models used to estimate 124 hydraulic soil properties, e.g. saturated hydraulic conductivity, on the basis of pedological 125 data [Wösten et al., 2001; Schaap et al., 2001], and are commonly derived empirically using 126 soil samples in continuum scale laboratory experiments where k, n, R, and  $\tau$  are measured 127 in bulk. Computational experiments with flow at the pore-scale allow these quantities to 128 be observed in detail and generalized pedotransfer functions to be empirically derived at 129 scales similar to those Kozeny and Carman considered but in more complicated networks. 130 The Kozeny (1) and and Kozeny-Carman (2) equations are generalized pedotransfer 131 functions for predicting permeability, a macroscopic soil property, derived analytically via 132 considerations of microscopic pore scale dynamics (they are general in the sense that the 133 predictors are not specific to a particular type of soil); Lebron et al. [1999] and Rawls 134 et al. [2005] provide comparisons between (1), (2) and other pedotransfer functions. 135

# 2.1. Permeability Based on Pore-scale Simulations

Computational solutions for the flow of a viscous fluid through an explicit pore space go 136 back at least to *Hasimoto* [1959] who solved for flow in a periodic array (cubic) of spheres 137 by deriving the fundamental solution to the Stokes equations using Fourier transforms. 138 He also obtained an expression for drag by expanding the velocity profile in terms of the 139 fundamental solution and its derivatives. Launder and Massey [1978] numerically solved 140 the Navier-Stokes equations for flow through a periodic array of long cylinders with known 141 geometric configurations. Sangani and Acrivos [1982a, b] and Zick and Homsy [1982] 142 computed Stokes drag on slow flows in porous media composed of simple elements like 143 spheres. Permeability has been estimated by simulating flow through more realistic pore 144

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networks by Lemaitre and Adler [1990], Fourie et al. [2007], [SW10], and Mostaghimi et al.
[2013] to name a few. Fourie et al. [2007] found good agreement between their numerical
estimates and measured permeabilities for a small volume of coarse sand (0.81 mm on a
side). Matyka et al. [2008] and [HSW12] found evidence for the existence of representative
elementary volumes in simulated flows through realistic random pore networks. Meakin
and Tartakovsky [2009] provide a current discussion of other methods for modeling flow
in porous networks.

The behavior of the Kozeny equation has been investigated through computational 152 experiments with flow in random or fractal pore networks. Scaling arguments indicate 153 good agreement between the Kozeny coefficient,  $c_0$ , and data obtained from computational 154 experiments with flow through networks based on Sierpinski carpets [Adler and Jacquin, 155 1987]. On the other hand, Adler et al. [1990] found that the Kozeny coefficient is about 156 half the standard value of 1/5 given by Carman [1939] when based on simulations of 157 flow through random media with statistics like Fontainbleau sandstone. Lemaitre and 158 Adler [1990] discovered that agreement between observed and theoretical values of the 159 Kozeny coefficient varied according to the porosity of networks they simulated: the Kozeny 160 equation did not hold for random media at relatively high or low porosities (in the latter 161 case, close to the percolation threshold they used to generate random media), nor did it 162 hold for media generated from regular fractals when the largest pores were held constant as 163 resolution was increased. The simulations performed in this paper also indicate nonlinear 164 behavior of permeability at high and low porosities, and also at extremes of mean hydraulic 165 radii. 166

#### 2.2. Physical Evidence for Kozeny Equation

The Kozeny and Kozeny-Carman equations have been validated and verified in experi-167 ments with flow through physical media composed of arrays of glass beads, other shapes 168 like rods, and natural porous media [Carman, 1956; Bear, 1988]. Soil scientists have 169 shown that (1) and (2) provide estimates of permeability that are superior to some other 170 soil transfer functions [Chapuis and Aubertin, 2003; Dvorkin, 2009]. The estimate given 171 by Carman [1939] of  $c_0 = 1/5$  for the Kozeny coefficient seems adequate for media in 172 a middle range of porosity (0.2 < n < 0.7) [Xu and Yu, 2008]. In some circumstances 173 high correlation between tortuousity and porosity makes the simpler Kozeny equation a 174 cost-effective alternative to the Kozeny-Carman equation [Koponen et al., 1996]. 175

The Kozeny and Kozeny-Carman equations have been found, however, to yield poor 176 estimates of permeability at the extremes of porous medium types: either when total fluid 177 discharge through a porous medium is negligible or at the other extreme where the effect 178 of the medium on the overall flow is local and small [Kyan et al., 1970; Xu and Yu, 2008]. 179 These results are consistent with the pore-scale computational experiments of *Lemaitre* 180 and Adler [1990] mentioned above and the experiments reported here. Heijs and Lowe 181 [1995] found that the Kozeny-Carman equation predicted the permeability of a particular 182 random array of spheres well (porosity n = 0.6), but failed to do so in a soil sample that 183 had porosity near one. Sullivan [1942], Kyan et al. [1970], Davies and Dollimore [1980] 184 and Xu and Yu [2008] all note that the Kozeny coefficient varies nonlinearly with porosity 185 and most significantly at its extreme values. 186

#### 2.3. Alternatives to Kozeny Equation

Efforts have been made to compensate for these weaknesses by modifying the Kozeny and Kozeny-Carman equations. The Kozeny-Carman equation has been expanded to include effective porosity [Koponen et al., 1997], percolation threshold and geometric properties of the pore network [Nabovati et al., 2009], and fractal geometry [Xu and Yu, 2008]. However Schaap and Lebron [2001] found that modifications do not always improve on estimates given by (1) and (2). Revil and Cathles [1999] derive a power-law relation,

$$k \propto d^2 n^{3m},\tag{3}$$

<sup>194</sup> between permeability of a clay-free sand, k, and grain diameter, d, and porosity, n, based <sup>195</sup> on an electrical cementation exponent, m, that reflects the connectivity of the pore space. <sup>196</sup> Their method depends on the Archie relationship [Archie, 1942],

$$n = \mathcal{F}^m, \tag{4}$$

that expresses porosity as a power of an electrical formation factor,  $\mathcal{F}$ , whose reciprocal quantifies the effective interconnected porosity of a porous medium. Values of m vary between 1 and 4 according to *Sen et al.* [1981]. *Revil and Cathles* [1999] derive power laws for permeability of a pure shale and sand-shale mixtures in a similar way with the specific value of m depending on the porous material. Jacquin [1964] quoted in [*Adler et al.*, 1990] found evidence for

$$k \propto n^{4.15} \tag{5}$$

for samples of Fontainbleau sandstone. *Lemaitre and Adler* [1990] indicate that permeability behaves like a power of porosity near the percolation limit (the value of porosity below which there are no continuous pore channels through one of their realizations) of

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the random porous media they construct. Other variants of the Kozeny equation that depend solely on porosity have been proposed by *Nielsen et al.* [1984] and *Ahuja et al.* [1989].

In sum, estimates of permeability based on the Kozeny and Kozeny-Carman equations 211 are reasonably accurate when applied to an intermediate range of porosities. This is true 212 for simulations based on pore-scale flows and physical experiments at laboratory scales. 213 For low porosity porous media like the Fontainbleau sandstone, shales, or sand-shale mix-214 tures, however, estimates of permeability based on the Kozeny equation are frequently 215 inaccurate, probably because linear dependence on porosity and the square of mean hy-216 draulic radius  $(R^2)$  does not completely capture the detailed effects of interconnectivity 217 within a pore network. When interconnectivity is accounted for by means of a formation 218 factor, permeability is fairly well captured by a power law based on porosity. The effect 219 that (squared) mean hydraulic radius has on permeability is not as well-established in the 220 literature as the effect of porosity. Revil and Cathles [1999] include it as a linear factor in 221 the porosity-based power law that they propose. 222

# 3. Simulation of Pore Network Flow and Permeability

First we provide the methods used to generate the virtual porous media and describe the physical data samples. Next, the procedure used to numerically integrate the Navier-Stokes equations within the explicit pore spaces is sketched, (see [SW10] for a complete description). Last, we detail the methods for observing and estimating variables of the pedotransfer functions.

# 3.1. Porous Media

The seventy-eight three dimensional porous media used as data sets for this study are comprised of a volcanic tuff, a column of glass beads, thirteen unique sandpacks, sandstones, and carbonates provided in Table 2 of *Mostaghimi et al.* [2013], and sixtythree realizations drawn from ensembles of virtual porous media with specified expected geometry and topology.

# <sup>233</sup> 3.1.1. Virtual Porous Media

Each virtual porous medium is a three-dimensional pore space with sides of length  $L_x = L_y = 1.27$  cm, height  $L_z = 2.55$  cm, and volume V = 4.11 cm<sup>3</sup> with individual pore areas typically 1-10  $\mu$ m<sup>2</sup> at a horizontal cross section. Level-set percolation [*Alexander and Molchanov*, 1994; *Alexander*, 1995] is used to generate realizations of porous media from underlying random topographies.

To generate each virtual pore space realization, independent identically distributed ran-239 dom values are sampled uniformly on the interval [0,1] and one value,  $f_i$ , is assigned to 240 each node, i, on a three-dimensional grid. Correlated random topographies are gener-241 ated from  $f_i$  using three different methods. In the first method,  $f_i$  is convolved with 242 a symmetric Gaussian kernel to generate an isotropic correlated random topography by 243 transforming  $f_i$  into frequency space, multiplying it by a Gaussian function, and then 244 transforming it back into real space. The correlation length of this random topography is 245 determined by the standard deviation of the Gaussian function which is fixed at  $\sigma = 0.01$ ; 246 see [HSW12] for details of this method. In the second method, a uniform kernel is ap-247 plied by uniformly weighting every point in a cube centered on  $\mathbf{x}$  with sides of length 248 l = 4. In the third method the random field  $f_i$  is low-pass filtered using m consecutive 249 applications of the tensor product  $f^{flt} = f^{fltx} \otimes f^{flty} \otimes f^{fltz}$ ; see [SW10] for details of 250

this method. Here, the symmetric weighting operator sweeps over  $f_i$  four times, m = 4. Values of  $\sigma = 0.01$ , l = 4, and m = 4 are chosen so the correlation lengths of realizations are approximately the same, ~ 0.05 cm. Since the convolution kernels have unit  $\mathcal{L}^2$  norm the convolutions do not change the expected value or range of the topographies. Moreover, the central limit theorem implies that all three methods yield topographies whose elements are approximately Gaussian.

A pore space realization is derived by applying a level threshold,  $\gamma \in [0,1]$ , to each 257 node value in the topography. If the value at the node is greater than  $\gamma$ , then the node 258 is placed in the solid matrix, otherwise it is in the void space. For physical intuition,  $\gamma$ 259 can be thought of as a control parameter which determines the expected porosity of a 260 pore space realization (Fig. 1), the exact linear relationship between the two is given in 261 Section II. A of [HSW12]. As  $\gamma$  increases, porosity and hydraulic radius also increase, while 262 tortuosity decreases (Table 1). The result of applying this level set percolation method is 263 a statistically stationary pore volume in the sense that the finite-dimensional probability 264 distributions of pore space membership are invariant with respect to translation in space. 265 The level threshold determines the flow volume, the geometric properties of porosity and 266 mean hydraulic radius, and topological properties such as the number of connected pore 267 channels and number of connected solid components. Another topological effect of the 268 level threshold is revealed by the existence of a percolation limit for topographies generated 269 by a given kernel, a threshold below which no amount of pressure will drive significant 270 flows through a pore space realization. At high values of the threshold parameter the flow 271 regime resembles slow flow around disconnected bodies with Reynolds numbers ranging 272 between 1 and 2. 273

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#### <sup>274</sup> 3.1.2. Physical Porous Media

The tuff data comes from a 0.34cm<sup>3</sup> sample volume with porosity 0.37 [Wildenschild 275 et al., 2004], and the glass beads are from a sample volume of  $0.032 \text{cm}^3$  with porosity 276 0.31 [Culligan et al., 2004]. Horizontal cross sections of these physical media are shown 277 in Fig. 2. Mostaghimi et al. [2013] obtain binarized three dimensional rock images of six 278 sandpacks, five sandstones, and two carbonantes using micro CT imaging, and determine 279 the permeability of the thirteen samples by numerically solving the Stokes equations in 280 the void space to attain steady state flow and pressure fields and then inverting Darcy's 281 law. The samples' porosity, specific surface, and permeability are provided in Table 2 282 of Mostaghimi et al. [2013]. 283

## **3.2.** Computational Fluid Dynamics

Flow in the virtual media is simulated by numerically solving the incompressible Navier-284 Stokes equations on a Cartesian domain with dimensions  $L_x = L_y = 1.27$  cm and  $L_z =$ 285 2.55 cm, and volume V = 4.11 cm<sup>3</sup>. The grids have 128 nodes in the horizontal directions 286 and 256 in the vertical direction. Computational limitations require that sub-volumes 287 of the beads and tuff be extracted from the center of the entire sample. Each medium, 288 whether virtual or physical, is periodic in the vertical direction with no flow allowed 289 across lateral boundaries. The real media are reflected across a horizontal plane to create 290 periodic boundaries in the vertical; Siena et al. [2012] demonstrated that this reflection 291 does not affect results. 292

The multi-scale computational fluid dynamics modeling system EULAG [*Prusa et al.*, 2008] is used to solve the governing Navier-Stokes equations for water flow, as in [*SW10*] and [*HSW12*], and the three components of velocity and pressure gradient are computed at every point within each porous medium. The EULAG system accommodates a broad
class of flows and underlying fluid equations in a variety of domains on scales ranging from
wind tunnel and laboratory [*Wedi and Smolarkiewicz*, 2006; *Smolarkiewicz et al.*, 2007; *Waite and Smolarkiewicz*, 2008] through terrestrial environments and climate [*Grabowski*and Smolarkiewicz, 2002; Abiodun et al., 2008a, b; Ortiz and Smolarkiewicz, 2009], to
stellar [*Ghizaru et al.*, 2010].

# <sup>302</sup> 3.2.1. Immersed Boundary Method

The crux of our computational approach for simulating flows in porous media is an 303 immersed-boundary method [Peskin, 1972; Mittal and Iaccarino, 2005] that inserts ficti-304 tious body forces into the equations of motion to mimic the presence of solid structures 305 and internal boundaries. The resulting dynamics are such that velocity is negligible and 306 pressure irrelevant within the solid matrix where the body forces are high. The particular 307 technique employed is a variant of feedback forcing [Goldstein et al., 1993], with implicit 308 time discretization admitting rapid attenuation of the flow to stagnation within the solid 309 matrix in  $\mathcal{O}(\delta t)$  time comparable to the time step  $\delta t = 5 \times 10^{-5}$  seconds of the fluid 310 model. The flow simulations are run for  $5 \times 10^{-2}$  seconds with steady state conditions 311 reached in  $2 - 3 \times 10^{-2}$  seconds. The complete description of this methodology for re-312 solving flow in explicit pore networks along with comparisons to other available methods 313 are in [SW10], [HSW12], and Siena et al. [2012]. Nonetheless, the concept behind this 314 method is provided for the reader's convenience. 315

<sup>316</sup> Since we focus on gravity-driven flows of a homogeneous incompressible fluid (e.g. wa-<sup>317</sup> ter) through a porous medium, the Navier-Stokes equations are,

$$\nabla \cdot \mathbf{v} = 0, \tag{6}$$

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$$\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} = -\nabla \pi' + \mathbf{g}' + \mu \Delta \mathbf{v} - \alpha \mathbf{v}.$$

The primes refer to perturbations with respect to static ambient atmospheric conditions characterized by a constant density,  $\rho_0$ , and pressure,  $p_0 = p_0(z)$ , so  $\pi' = (p - p_0)/\rho$  and  $\mathbf{g}' = (0, 0, -g\rho'/\rho)$  where  $\rho = \text{const} \gg \rho_0$  denotes the density of fluid and g is gravitational acceleration,  $\mathbf{g} = 9.81 \text{ m/s}^2$ . The kinematic viscosity of water,  $\mu$ , is  $10^{-6} \text{ ms}^{-2}$ .

The last term on the right hand side of the momentum equation is the fictitious repelling body force of the immersed-boundary method, with a non-negative time scale  $\alpha^{-1}(\mathbf{x}) = 0.5\delta t$  and the corresponding inverse time scale  $\alpha(\mathbf{x}) = 0$  within the solid and fluid, respectively. Intuitively, setting  $\alpha(\mathbf{x}) = 0$  within the fluid admits Navier-Stokes flows away from the solid boundaries, while requiring  $\alpha(\mathbf{x}) \to \infty$  within the solid assures  $\mathbf{v} \to 0$  there.

<sup>330</sup> Unlike other immersed boundary methods, the pore space boundaries are aligned with <sup>331</sup> grid nodes and the resulting media are simulated only with first-order accuracy in space. <sup>332</sup> However, the macroscopic uncertainty of microscopic pore structure greatly exceeds nu-<sup>333</sup> merical inaccuracies in the detailed representation of internal boundaries. Therefore, the <sup>334</sup> first order approximation of a porous medium is adequate, at least for determining sta-<sup>335</sup> tistical bulk properties of the media and flow.

# 3.3. Variables for Transfer Functions

<sup>336</sup> Porosity,

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$$n = V_P / V, \tag{7}$$

is the ratio of void volume,  $V_p$ , over bulk volume, V, and measures the relative capacity of a porous medium to hold water. Mean hydraulic radius,

$$R = V_P / A_i, \tag{8}$$

is the ratio the void volume over the total interstitial area between the pore space and the solid matrix,  $A_i$ , and indicates the average level of connectivity in the network. The tortuosity,

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$$\tau(a,b) = l_S/l,\tag{9}$$

of a fluid particle trajectory connecting two points a and b is the ratio of the trajectory length,  $l_S$ , over the Euclidean distance between its end points, l = ||a - b||, hence  $1 \leq \tau(a, b) < \infty$ . A number of alternate definitions are in use including  $\tau^2$ ,  $\tau^{-1}$ , and  $\tau^{-2}$ [Bear, 1988]. The average tortuosity,

$$\bar{\tau} = \frac{1}{N} \sum_{i=1}^{N} \tau(a_i, b_i),$$
(10)

is taken over a sample of i = 1, ..., N tortuosities,  $\tau(a_i, b_i)$ , each of which is derived from a particle trajectory that percolates through the entire medium. To determine the trajectory of a fluid particle, we follow [*HSW12*], and use every node in the void space at the top horizontal cross section as an initial position for a particle. To minimize the underestimation of tortuosity, only particles that percolate through the entire domain are included in the calculation of average tortuosity. The trajectory length,  $l_S$ , for every particle that percolates through the entire domain is used to compute tortuosity (9) and

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the average tortuosity for a pore space realization (10), cf., Section III. B of [HSW12] for a complete discussion.

<sup>359</sup> [*HSW12*] and *Matyka et al.* [2008] both demonstrated that average tortuosity (10) is <sup>360</sup> underestimated if the extent of the observation domain through which particles are tracked <sup>361</sup> is not sufficiently large. Furthermore, as the extent of the observation domain increases the <sup>362</sup> dependence on the extent of the domain decays exponentially, fluctuations in the computed <sup>363</sup> values diminish, and a representative elementary volume with respect to tortuosity is <sup>364</sup> observed for random virtual media.

Linear correlations among porosity, hydraulic radius, and tortuosity are significant 365 across the entire data set (Table 2). The porosities of the glass beads and tuff are com-366 parable to porosities for virtual media generated using the lowest value of the threshold 367 parameter. Tortuosities and hydraulic radii of the beads and tuff are also comparable to 368 those observed in the least permeable realizations of virtual media. The permeabilities 369 and hydraulic radii of the data provided in *Mostaghimi et al.* [2013] are two to four orders 370 of magnitude smaller than the stochastically generated pore networks used to derive the 371 power laws, but have porosities comparable to the lower end of the synthetic media. 372

#### 3.4. Permeability Estimates

Experimental estimates of permeability are obtained by applying Darcy's Law to the results of computational experiments with saturated pore spaces at steady state. By observing the pressure drop,  $\Delta p$ , and discharge of water, Q, from a column of sand of length L and cross-sectional area A, Darcy, [Darcy, 1856], established that discharge per unit area, Q/A, is proportional to the average pressure gradient,  $\Delta p/L$ , once steady-state X - 20 HYMAN, SMOLARKIEWICZ, WINTER: PEDOTRANSFER FUNCTIONS FOR PERMEABILITY 378 is reached,

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$$\frac{Q}{A} = -\frac{k}{\mu\rho} \frac{\Delta p}{L}.$$
(11)

The constant combines fluid density,  $\rho$ , and kinematic viscosity,  $\mu$ , with permeability, k, a material characteristic of a porous medium; the ratio  $K = k/(\mu\rho)$  is the saturated hydraulic conductivity of water according to Darcy.

Here, the permeability of each column of porous material bounded by solid walls on the lateral sides is estimated using the steady state velocity field,  $\mathbf{v} = (u, v, w)$ , and associated pressure field, p, of a fluid moving predominantly in the vertical direction. The total flux at a cross section of height z is estimated by

$$Q(z) = \int_{A} w(x, y, z) \chi(x, y, z) dx dy, \qquad (12)$$

where  $\chi$  is the characteristic (indicator) function within the porous material,  $\chi(x, y, z) = 1$ in the void space and  $\chi(x, y, z) = 0$  in the solid matrix. The total pressure is converted to hydraulic head,  $h = (p - p_o)/(\rho g) + z - z_o$ , where  $p_o$  is a reference pressure at the datum  $z_o$  and g is gravitational acceleration, and then the average hydraulic head at each cross section is estimated as

$$H(z) = \frac{1}{n(z)A} \int_A h(x, y, z) \chi(x, y, z) dx dy,$$
(13)

where n(z) is the porosity of the cross section at the level z. Expressing (11) in terms of (12) and (13) and rearranging terms, the permeability at each cross section is estimated

$${}_{6} \qquad \qquad k(z) = -\frac{\mu}{g} \frac{\int_{A} w(x, y, z) \chi(x, y, z) dx dy}{\Delta\{[n(z)]^{-1} \int_{A} h(x, y, z) \chi(x, y, z) dx dy\}/L}.$$
(14)

Because the dominant direction of flow is perpendicular to the cross sections, the average equivalent permeability for the entire sample is the harmonic average of the cross section

#### <sup>399</sup> permeabilities

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$$k_e = L_z \left( \int\limits_{L_z} \frac{1}{k(\zeta)} d\zeta \right)^{-1}.$$
 (15)

In practice, the support volume of this procedure is the horizontal cross section of each column with a vertical extent of three vertical grid levels. This volume is used to compute a second order accurate centered difference approximation of the hydraulic gradient in the vertical direction and the total flux (12) at each horizontal cross section.

# 3.5. Grid Resolution

In order to select a practical resolution for large numbers of flow simulations, a prelim-405 inary investigation is performed to determine how variations in grid resolution influence 406 the observed Darcy flux, q = Q/A (11), and estimated permeability,  $k_e$  (15). Because the 407 generation procedure of virtual media depends on the grid, a physical sample with fixed 408 resolution is used to assess the grid resolution effects. Using a sub-volume of the column 409 of glass beads, whose physical characteristics are discussed in Section 3.1.2, the grid is 410 refined and coarsened to four different levels. Linear interpolation is used to map the data 411 set between varying grid resolutions. Table 3 displays grid dimensions, discretization step 412 size,  $\delta x$ , mean Darcy flux, 413

$$\bar{q} \equiv \frac{1}{L_z} \int_{L_z} q(\zeta) d\zeta, \qquad (16)$$

average relative deviation from mean Darcy flux, Dev q, estimated permeability,  $k_e$ , average relative deviation from estimated permeability, Dev  $k_e$ , average tortuosity (10), and the variance of tortuosities for all four resolutions. Dev q and Dev  $k_e$  are defined as

Dev 
$$q \equiv \overline{|\bar{q} - q(z)|/|\bar{q}|}$$
 and Dev  $k_e \equiv \overline{|k_e - k(z)|/|k_e|}$ , (17)

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respectively, where the over-bar on the right hand side denotes vertical average as in (16). 419 Since the flow system is at steady-state, conservation of mass dictates that Dev q should 420 be zero. On the other hand, Dev  $k_e$  is not similarly constrained and finer resolutions should 421 yield better estimates of variations in permeability. The mean Darcy flux and estimated 422 permeability are about the same for all grid resolutions; whereas the values of Dev q are 423 relatively low, showing that conservation of mass is approximately satisfied, and improves 424 with grid resolution, approaching first order asymptotic convergence as pointed out in the 425 last paragraph of Section 3.2. The decreasing differences in average tortuosity and the 426 convergence of the variance of tortuosity at finer grid resolution also indicate that the 427 local flow field is better resolved with the finer mesh. 428

We supplement our convergence study for the integral characteristics of the Darcy flows 429 with a local convergence study for three randomly selected and substantially separated 430 locations in the vertical. Table 4 displays grid discretization size and the  $\mathcal{L}^2$  difference 431 between the probability distribution functions (pdf) generated by each component in the 432 velocity vector, (u, v, w), and the pdfs generated by velocity components at the finest 433 resolution. For each of the velocity components at all three levels the relative error from 434 the finest mesh resolution solution exhibits the aforementioned first order convergence. 435 Moreover, the error between finest and second finest resolution is small. Therefore, we 436 select the second most refined grid,  $\delta x = 1.e^{-4}$ m, for computational affordability. 437

# 4. Generalized Pedotransfer Functions

The data consist of triples  $(k_i, n_i, R_i)$  for each of the i = 1, ..., 63 virtual pore spaces. Models, whose parameters are fitted through least squares, produce an estimate,  $\hat{k}_i = \hat{k}(\eta_i)$ , of permeability with  $\eta$  referring to  $n, R^2$ , or  $nR^2$ . To evaluate the performance of the models the independent real media data are withheld from the fitting and used to evaluate the goodness-of-fit through plots and overall chi-squared tests.

## 4.1. Empirical Pedotransfer Functions

When the data are fitted to the Kozeny equation (1), the Kozeny coefficient is  $c_0 = 0.19$ , 443 which is essentially the same as Carman's original value of 1/5 [Carman, 1939] and falls 444 within the range [1/6, 1/2] that he gave later [Carman, 1956]. However, the relationship 445 between permeability and the Kozney predictor is nonlinear over the ranges of sample data 446 (Fig. 3). The Kozeny equation captures the basic rising trend of permeability with the 447 Kozeny predictor,  $nR^2$ , but the requirement that the model goes through the origin, which 448 is a necessary condition for a physically consistent law, constrains the performance of the 449 Kozeny equation. The best fit linear model to these data, which is not shown, has a linear 450 correlation of 0.9, but it does not go through the origin. The nominal 95% confidence 451 intervals for the Kozenv equation are so wide that they easily include the independent 452 real data. Confidence intervals are nominal in the sense that classic statistical formulae 453 are used to calculate them, but the data do not meet independence and distributional 454 criteria for statistical hypothesis testing. Nonetheless, the confidence intervals are useful 455 for comparisons. For these purposes, a useful confidence interval is narrow, yet includes 456 nearly all the data. 457

<sup>458</sup> A better fit to the data can be attained using nonlinear models based on porosity n, <sup>459</sup> hydraulic radius  $R^2$ , and their product  $nR^2$ . Three power law models to predict perme-<sup>460</sup> ability,  $\hat{k}(\eta) = a(\eta)^b$ , are derived and compared to the linear Kozeny equation. The free <sup>461</sup> parameters a and b are fitted using the nonlinear fit module in MATHEMATICA [Wol-<sup>462</sup> fram, 1999]. Due to the high correlation of tortuosity  $\tau$  with n and  $R^2$ ,  $\tau$  is not used as

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<sup>463</sup> a predictor variable in the power laws. All three power laws capture the nonlinear trend <sup>464</sup> of the data and their confidence intervals are fairly tight including the independent real <sup>465</sup> data (Fig. 4-6).

466 The sum of squared departures of the simulated data,  $\hat{k}$ , from the model estimates,

$$s_d^2 = \sum_{i=1}^{N_s} (\hat{k}_i - k_i)^2, \tag{18}$$

is the total variability in the data that is not accounted for by the models where  $N_s$  is the number of samples ( $N_s = 63$  for this data set). The sum of squared departures of the Kozeny equation is an order of magnitude greater than those of the power laws (Table 5). The additional parameter is one reason the power laws perform better than the Kozeny equation. A statistical method, the Analysis of Variance [*Mood et al.*, 1963], takes this into account by weighting the sum of squared departures with P, the number of parameters in the model, and comparing it to the model sum of squares,

$$s_M^2 = \sum_{i=1}^{N_s} (\hat{k}_i - \langle k \rangle)^2, \tag{19}$$

weighted by  $N_s - P$ , the degrees of freedom remaining in the sample after accounting for the parameters. The model sum of squares reflects the ability of the model to capture the structure of the data as departures from the sample mean,  $\langle k \rangle$ . The ratio,

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$$F = \frac{s_M^2 / P}{s_d^2 / (N_s - P)},$$
 (20)

can be used to compare models: the larger is F, the better is the fit of the model. The F ratios of the predictor power law is about four times greater than that of the Kozeny equation despite the additional parameter (Table 6). The F ratios for the power laws based solely on n or  $R^2$  are triple and double that of the Kozeny equation.

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#### 4.2. Range of Applicability

Porous media may fall into three classes. The first class consists of ordinary porous 484 media with porosities in the approximate range 0.2 < n < 0.7. In these cases, porosity 485 is primary in the sense that it arises from voids in the material of the medium. In the 486 second class there are barely permeable media with low porosities, n < 0.2. Often such 487 media are composed of nearly solid rock with secondary channels arising from external 488 mechanical or thermal stresses [Davis, 1988]. In these cases flow often corresponds to flow 489 through a collection of discrete, sparsely connected pipes. Finally, the third class consists 490 of highly permeable media where flow is similar to slow flows with obstructions that are 491 relatively widely spaced, for instance fluidized beds. The porous media investigated here 492 fall into either the first or third class. 493

When restricted to media of the first class, porosities 0.2 < n < 0.7, a version of the Kozeny equation

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$$k = 0.35nR^2,$$
 (21)

<sup>497</sup> provides reasonable estimates of permeability in agreement with the conclusions of Xu<sup>498</sup> and Yu [2008]. In this range, the model (21) also provides a close fit to the real data <sup>499</sup> (Fig. 7). Moreover, the computed Kozeny coefficient,  $c_0 = 0.35$ , is within the range <sup>500</sup>  $1/6 < c_0 < 1/2$  given by *Carman* [1956]. Within this normal range of porosity, the <sup>501</sup> Kozeny-Carman equation (2) is

$$k = 0.45nR^2/\tau^2.$$
 (22)

<sup>503</sup> Carman [1956] mentions  $c'_0 = 0.40$  is plausible for non-circular sections.

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The *F* ratio (20) for model (21) is F = 1770.55, which is greater than the *F* ratio obtained for the power laws based upon *n* or  $R^2$  and thrice as large as that for the Kozeny equation fitted to the entire data set. However, the F ratio of model (22), F = 551.09, is less than half of that of (21).

The Kozeny equation does not account for variability over the full range of data as well as the power laws, having a sum of squared errors that is an order of magnitude greater than the power law models (Table 5). This is true even when the model sums of squares are adjusted for the number of parameters (Table 6).

<sup>512</sup> Of the four models considered here, the power law based on the Kozeny predictor,

$$\hat{k} = 1.68 \cdot 10^{-4} (nR^2)^{0.58},\tag{23}$$

fits the entire virtual data set best having an F ratio of 1866.17, which is nearly four times that of the Kozeny equation over the entire set and roughly double that of (21). Power laws based on porosity and hydraulic radius, the components of the Kozeny predictor, also give good fits to all the data. The exponent appears to account for nonlinear effects at the extremes of pore space interconnectivity consistent with observations of Jacquin [1964] quoted in [Adler et al., 1990], Lemaitre and Adler [1990] and Revil and Cathles [1999].

Figures (3-6) indicate that the power-law models and the Kozeny equation fit the inde-521 pendent observed data well. However, the power-law based on porosity alone does not fit 522 the low permeability samples obtained from *Mostaghimi et al.* [2013] as well as the other 523 models. Nonetheless, the power laws are clearly superior to the Kozeny equation when 524 the goodness of model fits is evaluated by chi-squared tests applied to both observed and 525 virtual data (Table 7). Chi-squared tests are based on distances between model estimates 526 and data weighted by the estimates [Mood et al., 1963], and are used here qualitatively 527 in the same spirit as the Analysis of Variance results reported earlier (Table 6). Small 528

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values of the chi-squared statistic indicate good fits, and the chi-squared values for the power laws are about five-six times smaller than the corresponding value for the Kozeny equation.

# 5. Summary and Conclusions

Kozeny derived his equation by equating the velocity given by Poiseuille's law for flow 532 through an idealized pore network to the specific discharge obtained via Darcy's law; he 533 determined that the permeability of a porous medium, k, is linearly proportional to the 534 product  $nR^2$  of its porosity, n, with the square of its mean hydraulic radius, R. This 535 simplified model of a porous medium allowed him to attain an analytical solution to the 536 governing equations of flow through porous media. However, topological alterations that 537 make a pore network more realistic render analytical solutions nearly intractable. When 538 applied over a wide range of porous media, computational experiments reveal a nonlinear 539 relationship between permeability and its predictors, contrary to Kozeny's result. This 540 nonlinearity is manifested by the wide range of values of the Kozeny coefficient observed 541 at the extreme ends of porosity [Sullivan, 1942; Kyan et al., 1970; Davies and Dollimore, 542 1980; Adler et al., 1990; Xu and Yu, 2008]. On one hand, Kozeny's linear (in the predictor 543  $nR^2$ ) approximation appears satisfactory within a restricted range of porosities, 0.2 < n < 1544 0.7. On the other hand, the nonlinearity cannot be adequately represented by a linear 545 approximation when a wider range of porosity is considered. 546

<sup>547</sup> We empirically derive three nonlinear generalized pedotransfer functions for permeabil-<sup>548</sup> ity using computational experiments with flow through a set of stochastically generated <sup>549</sup> pore networks with porosities ranging from 0.19 to 0.84 and varying degrees of connec-<sup>550</sup> tivity. The transfer functions are power laws based on porosity n, mean hydraulic radius <sup>551</sup> squared  $R^2$ , and their product  $nR^2$ ; the same predictor which Kozeny used. The ex-<sup>552</sup> perimental pore networks consist of sixty-three virtual networks whose permeabilities, <sup>553</sup> porosities, and mean hydraulic radii are used to estimate the parameters of the transfer <sup>554</sup> functions. Porosity and mean hydraulic radius are observed directly from images of the <sup>555</sup> pore networks and Darcy's law is used to compute the permeability from steady-state flow <sup>556</sup> fields within the porous media.

When fitting the Kozeny equation to the full range of data, the computed value of the 557 Kozeny coefficient computed is  $c_0 = 0.19$ , essentially the value originally suggested by 558 Carman,  $c_0 = 1/5$  [Carman, 1939]. However, the Kozeny equation does not provide good 559 estimates of permeability over the full range of data, because of the nonlinear dependence 560 of k on the Kozeny predictor,  $nR^2$ . On the other hand, the Kozeny equation is reasonably 561 accurate within a limited range of of porosities (Fig. 7), but not for the originally suggested 562 value of the Kozeny coefficient. Nonetheless, the estimated value of  $c_0 = 0.35$  is within 563 the wider range  $1/6 < c_0 < 1/2$  that Carman gave later [Carman, 1956]. 564

All of the transfer functions include the fifteen independent real data samples within 565 nominal 95% confidence intervals. The power laws fit the data in this study better than 566 the Kozeny equation, even when they are penalized through an Analysis of Variance for 567 including an additional model parameter (Table 5-6). The leading coefficient of each 568 power law is an empirical fitting parameter and has dimensions of  $L^{2(1-b)}$ , where b is the 569 power appearing in Table 5. Only in specialized cases, such as the Kozeny equation are 570 the associated coefficients dimensionless. Similar functions to predict permeability having 571 coefficients with dimensions are already present in the literature [Katz and Thompson, 572 1986; Ahuja et al., 1989; Rodriguez et al., 2004; Costa, 2006]. 573

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574 The equation

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$$\hat{k} = 1.68 \cdot 10^{-4} (nR^2)^{0.58} \tag{24}$$

provides the best fit to the full range of data. Additionally, its confidence intervals are tighter, its sum of squared departures is smaller, and its F (20) ratio is higher than any of the other models considered.

Even though Kozeny derived his equation through microscopic considerations, it has been applied on macroscopic scales as a generalized pedotransfer function. Commonly, pedotransfer functions are derived empirically using various soil samples in continuum scale laboratory experiments where the predictors, e.g., porosity and mean hydraulic radius, can be measured in bulk.

The virtual networks that are the basis for these transfer functions are homogeneous 584 and isotropic with porosities and mean hydraulic radii spanning a wide range of repre-585 sentative values. Sample permeabilities are comparable to those found in well- sorted 586 sands or sands and gravel. Since the networks are large enough to constitute represen-587 tative elementary volumes [HSW12], the physical basis and scale of these experiments 588 is comparable to that which Kozeny used. Moreover, the derived pedotransfer functions 589 are not formally limited to representations of explicit pore spaces or a particular soil type 590 because porosity and hydraulic radius can be estimated in bulk using field observations 591 or laboratory experiments and are general traits of porous media. As a result, it should 592 be possible to test whether the proposed generalized pedotransfer functions apply in the 593 field. 594

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Acknowledgments. We wish to thank Dorthe Wildenschild of Oregon State Univer-595 sity for generously sharing her tuff and bead data sets with us. We also thank an anony-596 mous referee for bringing the recently published data of *Mostaghimi et al.* [2013] to our 597 attention. We also want to thank Alberto Guadagnini, Monica Riva, and Martina Siena 598 for commenting on early drafts of this paper and Shlomo Neuman for several discussions. 599 J.D.H. acknowledges the support of the Graduate Visitor Program, a part of the Advanced 600 Study Program at the National Center for Atmospheric Research. P.K.S acknowledges 601 partial support by the DOE awards #DE-FG02-08ER64535 and #DE-SC0006748, and 602 the NSF grant OCI-0904599 while conducting this work. The National Center for Atmo-603 spheric Research is sponsored by the National Science Foundation. 604

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Figure 1. Porespace cross-sections in the x-y plane (1.27 cm  $\times$  1.27 cm). From left to right : uniform kernel, Gaussian kernel, and iterative method; top, Threshold Parameter 0.45 (Expected Porosity  $\approx 0.35$ ); bottom, Threshold Parameter 0.53 (Expected Porosity  $\approx 0.60$ ).



Figure 2. Physical porous media: tuff (left) and glass beads (right); corresponding values of  $(n, \tau, R)$  are (0.37, 1.23, 9.12·10<sup>-5</sup> m) and (0.31, 1.20, 2.89·10<sup>-5</sup> m.)



Figure 3. Kozeny equation  $k(nR^2) = c_0 nR^2$ . Points correspond to averaged amounts for each of the 63 stochastic realizations and fifteen sets of natural data. Circles, blue square, red triangle, and green diamonds denote synthetic data, glass beads, tuff, and the low permeability data of *Mostaghimi et al.* [2013] respectively. Least-squares models are solid lines, and nominal 95% confidence intervals are dashed lines.



Figure 4. As in Fig. 3 but for power law  $k(R^2) = a(R^2)^b$ .



**Figure 5.** As in Fig. 3 but for power law  $k(n) = an^b$ .



Figure 6. As in Fig. 3 but for power law  $k(n) = a(nR^2)^b$ .



Figure 7. Kozeny equation fitted to porous media with normal porosities, 0.2 < n < 0.7; Circles, square, triangle, and diamonds denote synthetic data, glass beads, tuff, and the low permeability data of *Mostaghimi et al.* [2013] respectively.

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			Uniform	Gaussian	Iterative
		$\gamma =$	0.45 (Exped	cted Porosity	$y \approx 0.35)$ :
		$k^{\mathrm{a}}$	$1.10 \cdot 10^{-9}$	$1.32 \cdot 10^{-9}$	$9.10 \cdot 10^{-10}$
		$n^{\mathrm{b}}$	0.43	0.38	0.36
		$R^2$ c	$5.16 \cdot 10^{-9}$	$7.63 \cdot 10^{-9}$	$7.33 \cdot 10^{-9}$
		$nR^2 d$	$2.22 \cdot 10^{-9}$	$2.94 \cdot 10^{-9}$	$2.68 \cdot 10^{-9}$
		au e	1.25	1.23	1.33
		$\gamma =$	0.53 (Expection)	cted Porosit	$y \approx 0.60)$ :
			0		0
		$k^{a}$	$3.00 \cdot 10^{-9}$	$4.76 \cdot 10^{-9}$	$5.26 \cdot 10^{-9}$
		n <sup>b</sup>	0.60	0.62	0.68
		$R^2$ c	$1.05 \cdot 10^{-8}$	$1.97 \cdot 10^{-8}$	$2.88 \cdot 10^{-8}$
		$nR^2$ d	$6.30 \cdot 10^{-9}$	$1.22 \cdot 10^{-8}$	$1.97 \cdot 10^{-8}$
		au e	1.16	1.12	1.14

 Table 1.
 Characteristics of virtual media in Fig. 1.

- <sup>a</sup> Permeability [m<sup>2</sup>]
- <sup>b</sup> Porosity
- <sup>c</sup> Hydraulic radius squared [m<sup>2</sup>]
- <sup>d</sup> Kozeny predictor [m<sup>2</sup>]
- <sup>e</sup> Tortuosity

 Table 2.
 Correlations among predictor variables.

	n	R	au
$\overline{n}$	1.00	0.90	-0.95
R	0.90	1.00	-0.84
au	-0.95	-0.84	1.00

$n \times m \times l^{a}$	$\delta x^{ m b}$	$ar{q}$ c	Dev $q \ [\%]$	$k_e^{e}$	Dev $\mathbf{k}_e$ [%] f	$ar{ au}^{ m g}$	$\sigma(\tau)^{\rm h}$
$18 \times 18 \times 38$	4.e-04	-2.00e-02	1.16	2.04e-09	121.86	1.25	1.54e-02
$36 \times 36 \times 76$	2.e-04	-2.08e-02	0.86	2.12e-09	117.08	1.28	2.11e-02
$72 \times 72 \times 150$	1.e-04	-2.12e-02	0.39	2.16e-09	202.41	1.31	2.21e-02
$144 \times 144 \times 300$	5.e-05	-2.02e-02	0.22	2.06e-09	215.61	1.31	2.22e-02

Table 3.Grid Resolution Study

<sup>a</sup> Grid dimensions

- <sup>b</sup> Grid discretization [m]
- <sup>c</sup> Mean Darcy flux [m/s]
- <sup>d</sup> Average relative deviation from the mean Darcy flux [%]
- <sup>e</sup> Estimated permeability  $[m^2]$
- <sup>f</sup> Average relative deviation from estimated permeability [%]
- <sup>g</sup> Average Tortuosity
- <sup>h</sup> Variance of Tortuosities

 Table 4.
 Local Grid Resolution Study

		Level 1			Level 2			Level 3	
$\delta x^{a}$	$L^2(u)$ b	$L^2(v)$ <sup>c</sup>	$L^2(w) d$	$L^2(u)$ b	$L^2(v)$ <sup>c</sup>	$L^2(w)^{\mathrm{d}}$	$L^2(u)$ b	$L^2(v)$ <sup>c</sup>	$L^2(w) d$
4.e-04	1.73e-01	1.44e-01	1.15e-01	1.48e-01	1.14e-01	1.19e-01	1.46e-01	1.22e-01	1.04e-01
2.e-04	7.33e-02	7.01e-02	5.65e-02	6.41e-02	5.25e-02	5.20e-02	7.36e-02	6.93e-02	5.50e-02
1.e-04	3.39e-02	4.10e-02	3.25e-02	3.07e-02	2.75e-02	3.24e-02	3.20e-02	3.14e-02	2.98e-02

- <sup>a</sup> Grid discretization [m]
- <sup>b</sup>  $L^2$  difference between pdf of u and pdf of u at finest resolution
- <sup>c</sup>  $L^2$  difference between pdf of v and pdf of v at finest resolution
- <sup>d</sup>  $L^2$  difference between pdf of w and pdf of w at finest resolution

Table 5.Accuracy of the four fitted models.

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Model Form	$\operatorname{Fit}$	$s_d^2$
$k(nR^2) = c_0 nR^2$	$\hat{k} = 0.19 n R^2$	$2.26 \cdot 10^{-16}$
$k(nR^2) = a(nR^2)^b$	$\hat{k} = 1.68 \cdot 10^{-4} (nR^2)^{0.58}$	$3.15 \cdot 10^{-17}$
$k(n) = an^b$	$\hat{k} = 1.72 \cdot 10^{-8} (n)^{2.83}$	$3.72 \cdot 10^{-17}$
$k(R^2) = aR^{2b}$	$\hat{k} = 1.37 \cdot 10^{-3} (R^2)^{0.71}$	$5.61 \cdot 10^{-17}$

 Table 6.
 Analysis of Variance

Model	P	$s_M^2/P$	$N_s - P$	$s_d^2/(N_s - P)$	F
Kozeny eq.	1	$1.74 \cdot 10^{-15}$	62	$3.65 \cdot 10^{-18}$	475.77
power law $k(nR^2)$	2	$9.65 \cdot 10^{-16}$	61	$5.16 \cdot 10^{-19}$	1866.17
power law $k(n)$	2	$9.62 \cdot 10^{-16}$	61	$6.11 \cdot 10^{-19}$	1574.55
power law $k(R^2)$	2	$9.52 \cdot 10^{-16}$	61	$9.20 \cdot 10^{-19}$	1034.89

 Table 7.
 Chi Squared Statistics

Model	$\chi^2$ Statistics
Kozeny eq.	$7.57 \cdot 10^{-08}$
power law $k(nR^2)$	$1.12 \cdot 10^{-08}$
power law $k(n)$	$1.19 \cdot 10^{-08}$
power law $k(R^2)$	$1.76 \cdot 10^{-08}$